Memories
Bipolar Transistors

Exams

February 5
March 7
April 18
June 27

Exam

Four questions, two from the online list.

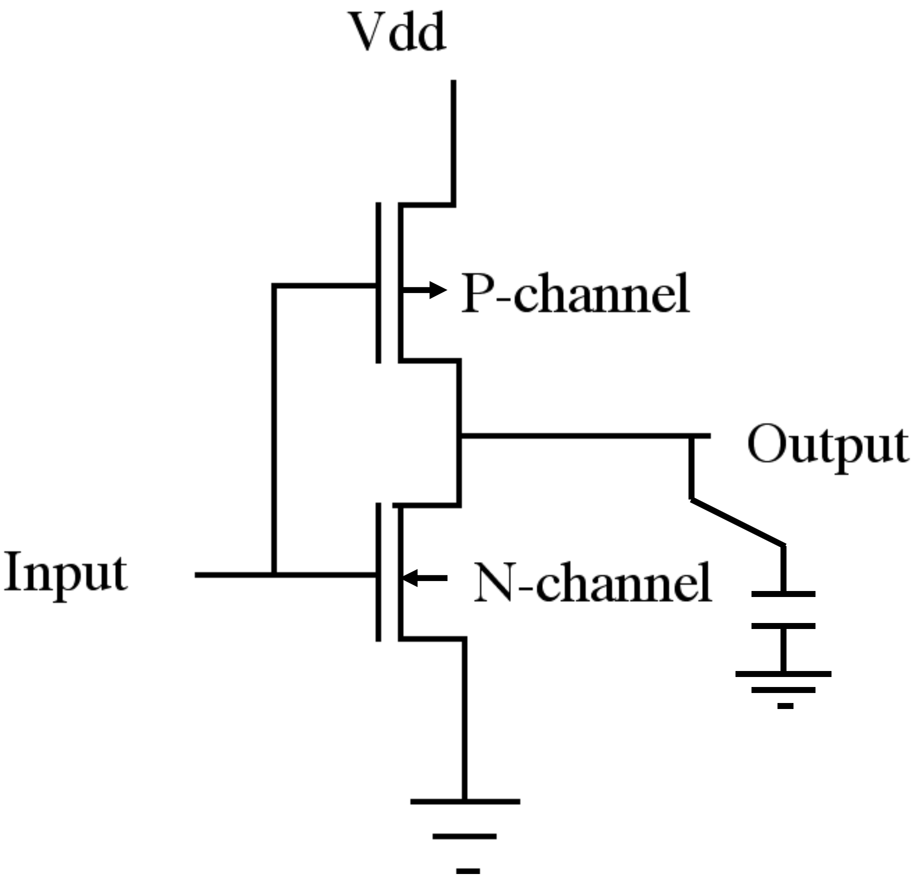
Calculator is ok. No notes.

Explain some concept:
(tunnel contact, indirect band gap, thermionic emission, inversion, threshold voltage, ...)

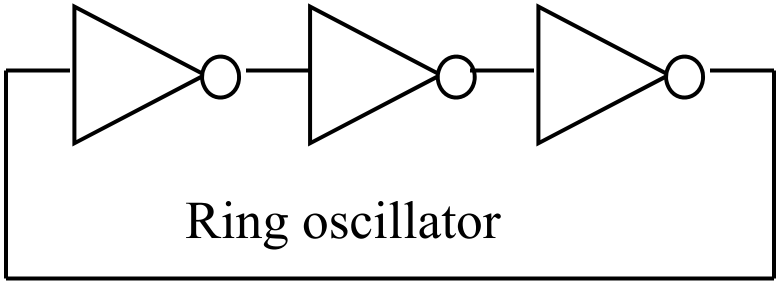
Perform a calculation:
(concentration of minority carriers, integrate charge density to find electric field, ...)

Explain how a device works:
(JFET, MESFET, MOSFET, laser diode, bipolar transistor, LED, Schottky diode, Heterojunction bipolar transistor, ...)

Gate delay

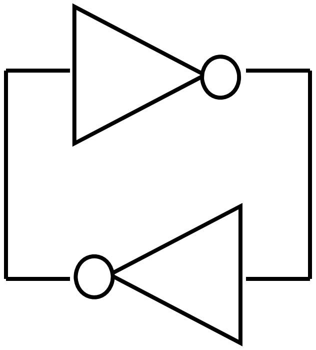


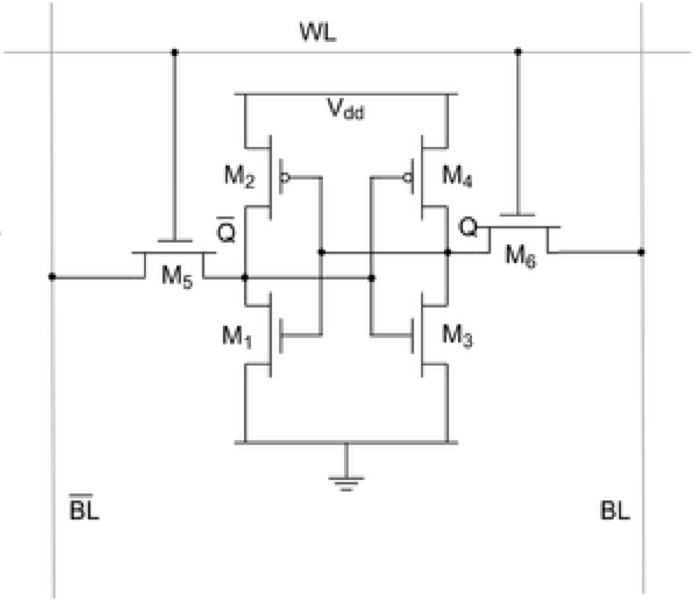
Gate delay is limited by $C_{gate}V_{dd}/I$.


Ring oscillator

SRAM

Static random access memory

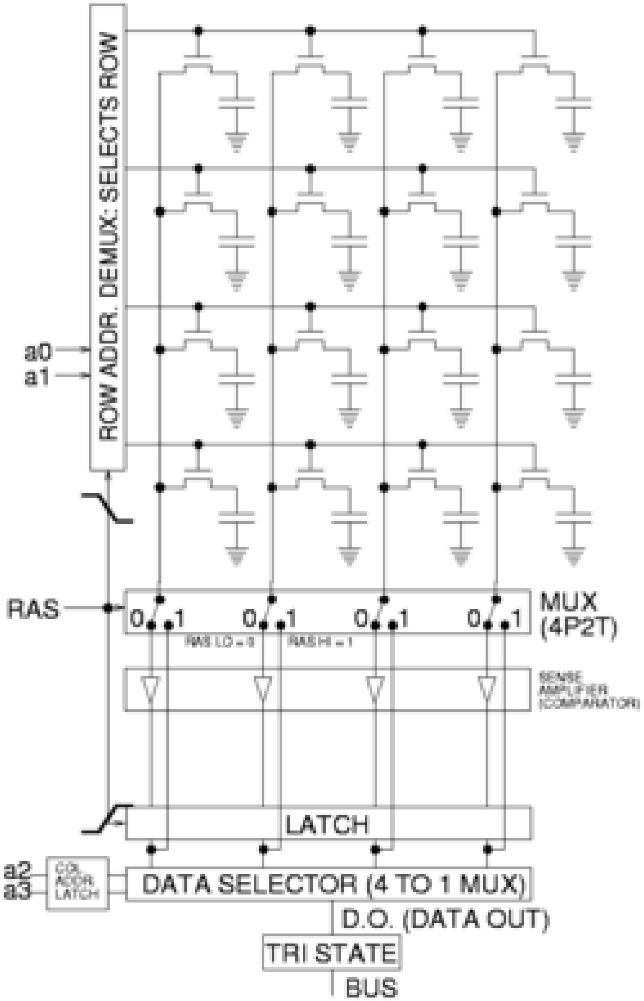




No refresh circuitry needed.

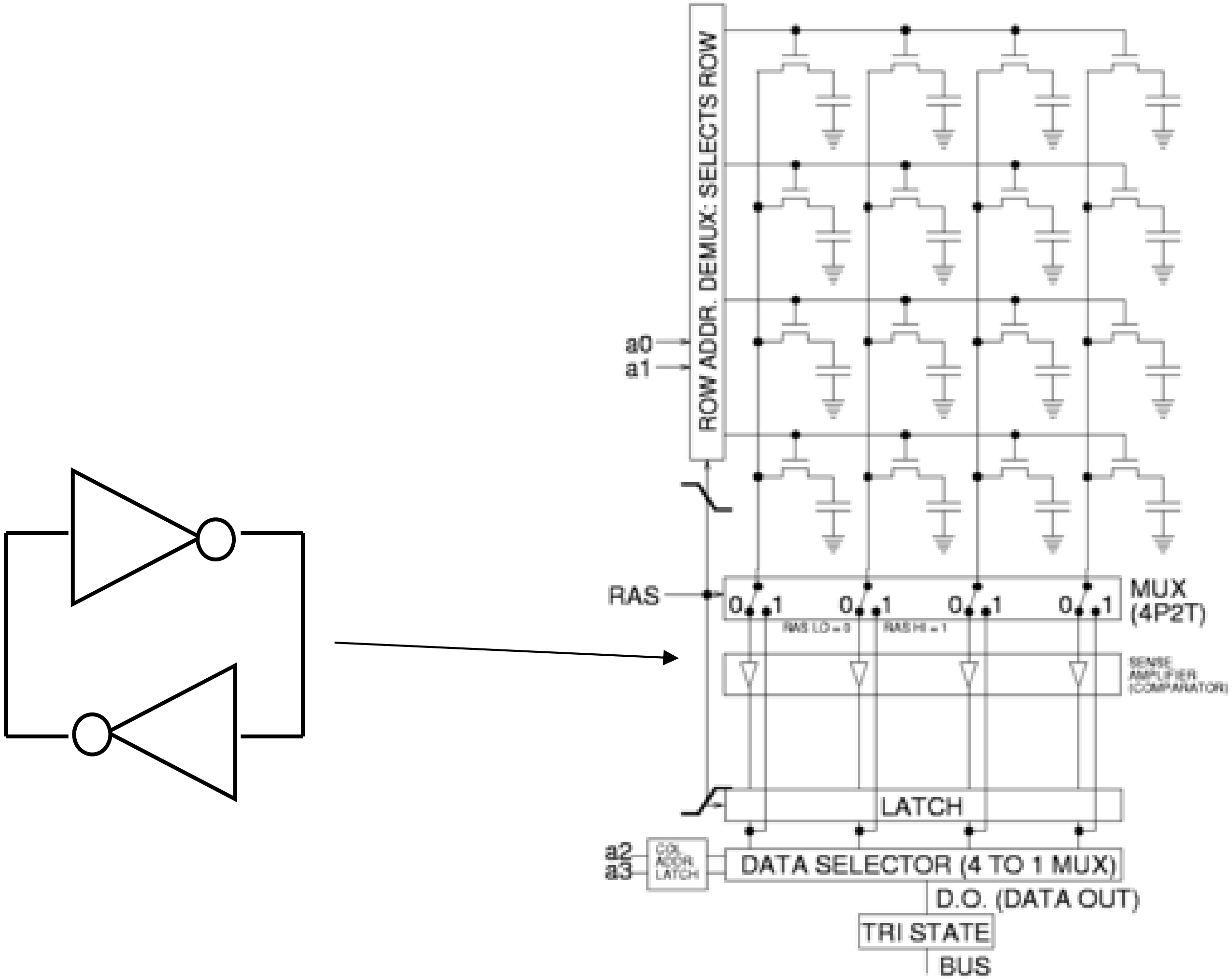
DRAM

Dynamic random access memory

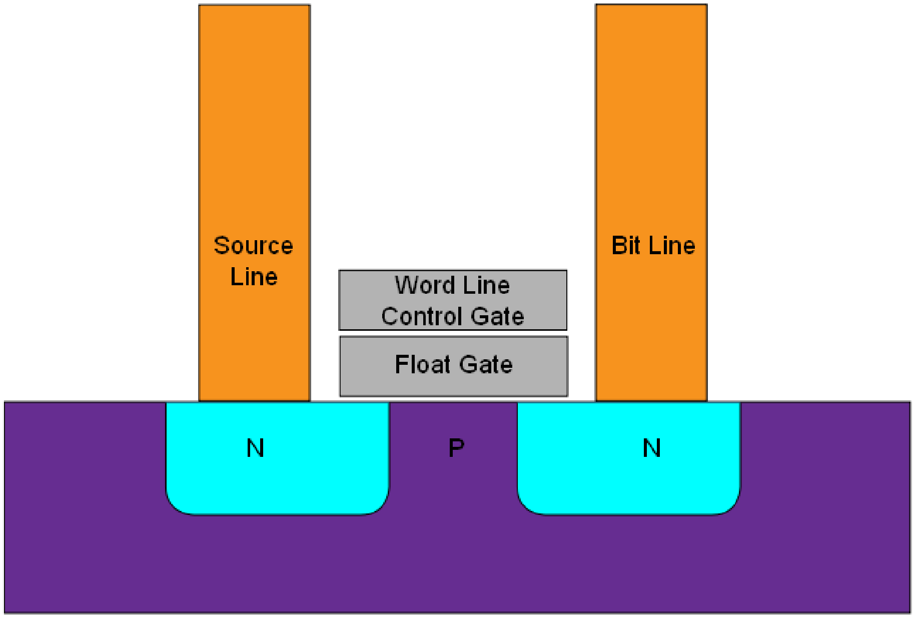


DRAM

Read and refresh DRAM with a SRAM cell



Flash memory



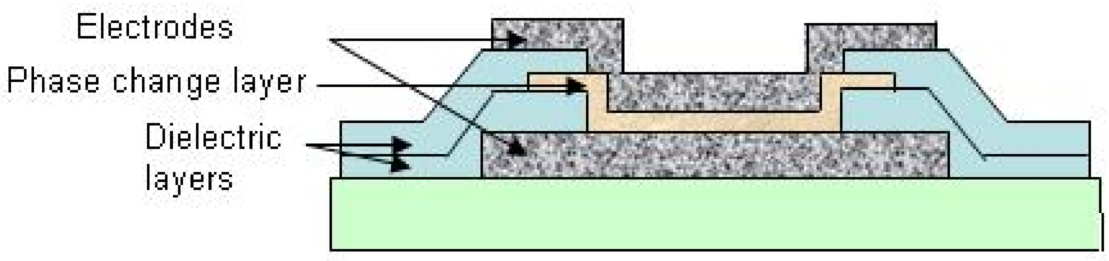
Charge is stored on a floating gate

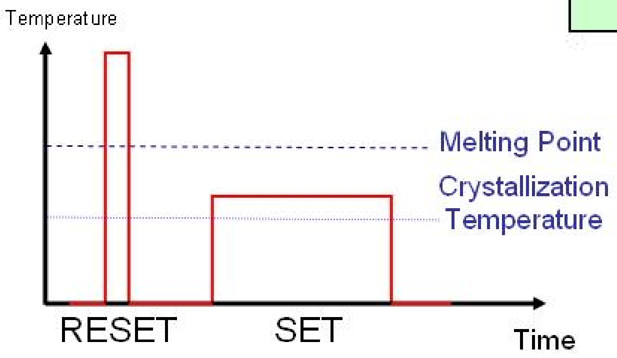
nonvolatile

Phase change memory

Phase-change memory (PRAM) uses chalcogenide materials. These can be switched between a low resistance crystalline state and a high resistance amorphous state.

GeSbTe is melted by a laser in rewritable DVDs and by a current in PRAM.

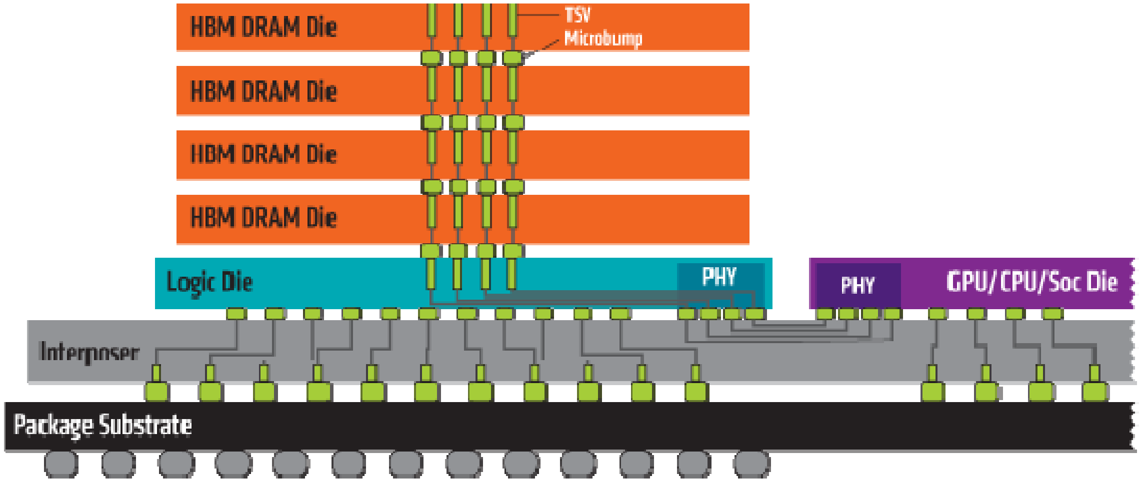


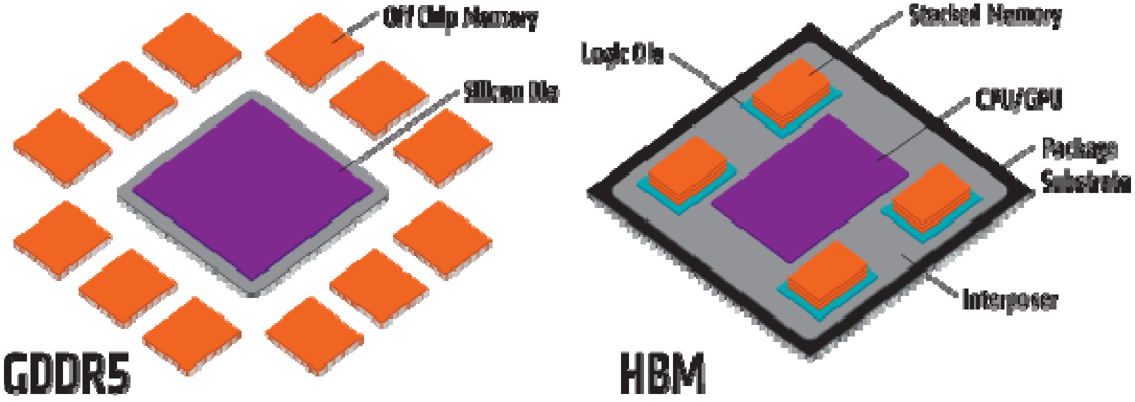


nonvolatile

High Bandwidth Memory

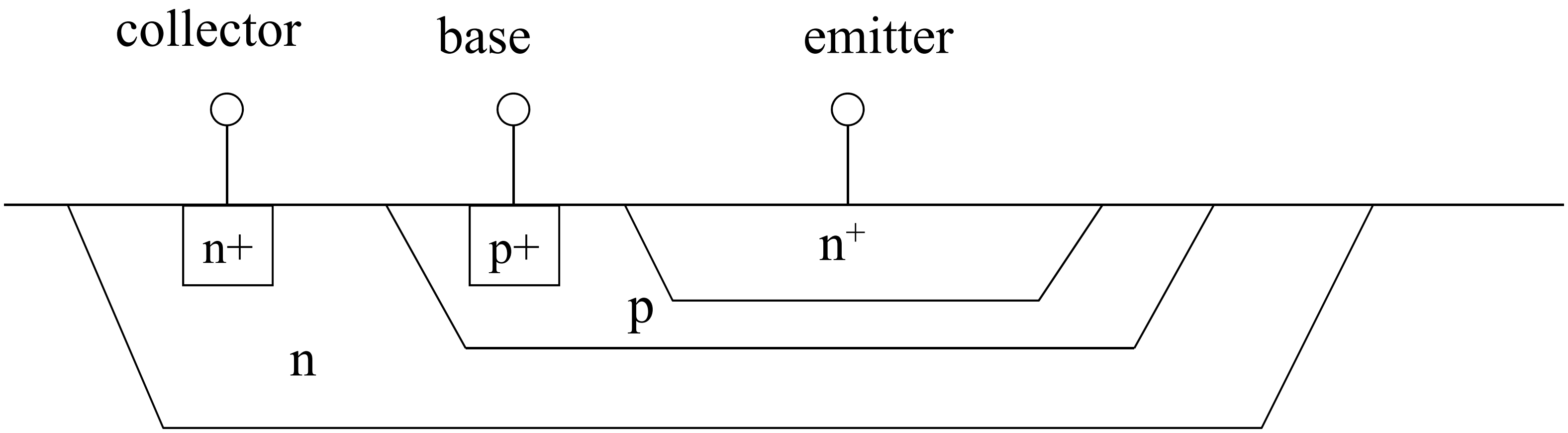
AMD to launch its HBM graphics cards on 16 June 2015.





bipolar transistors

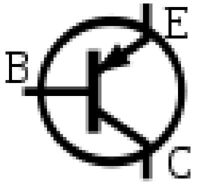
npn transistor



lightly doped p substrate

Used in front-end high-frequency receivers (mobile telephones).

bipolar transistors



PNP

NPN

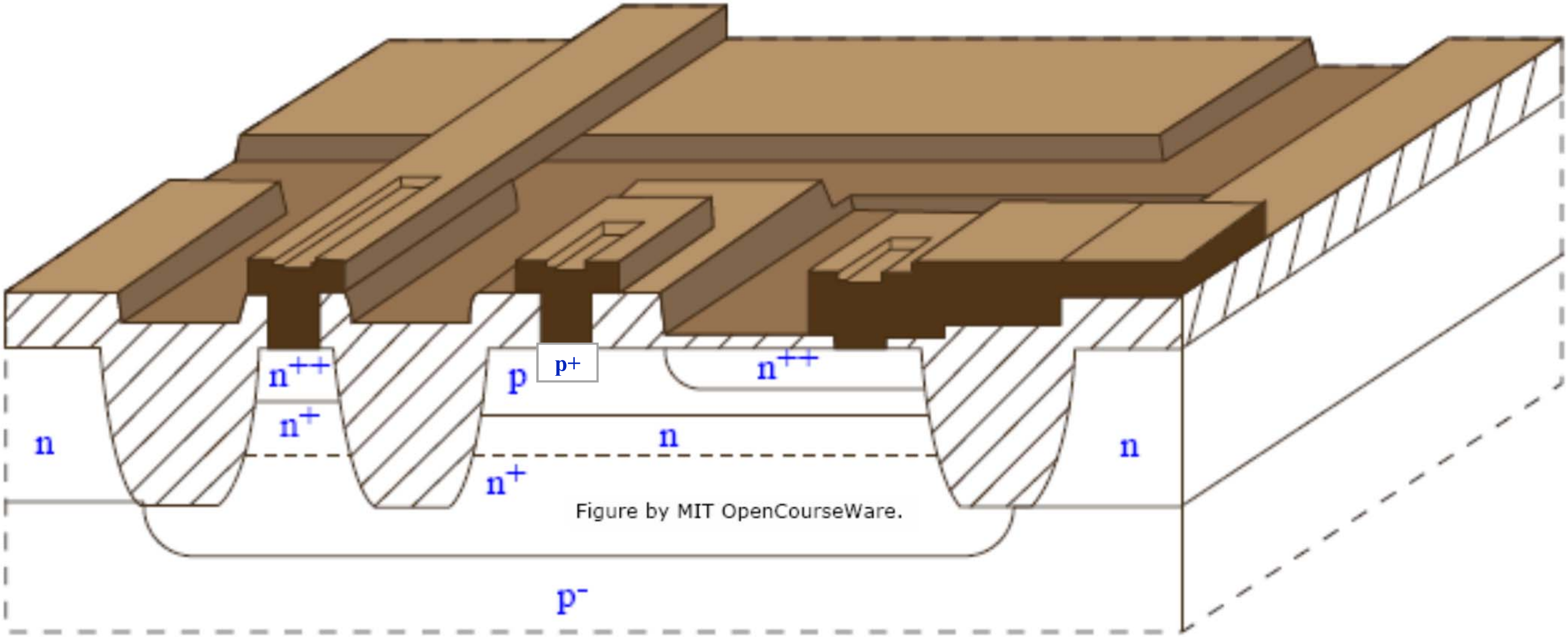
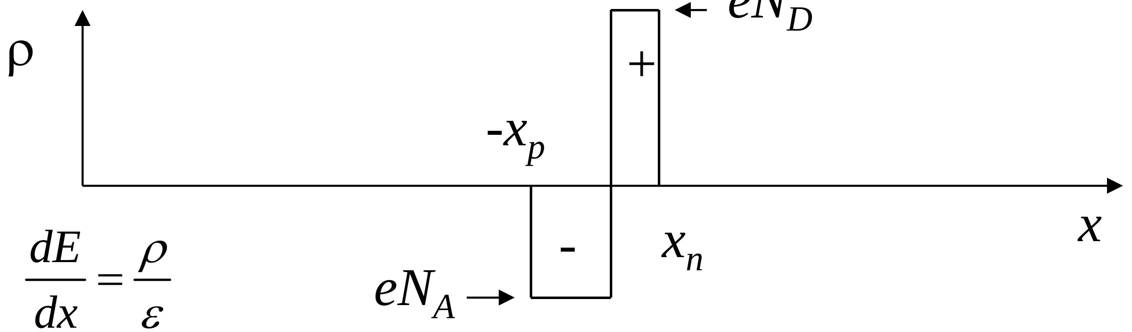


Figure by MIT OpenCourseWare.

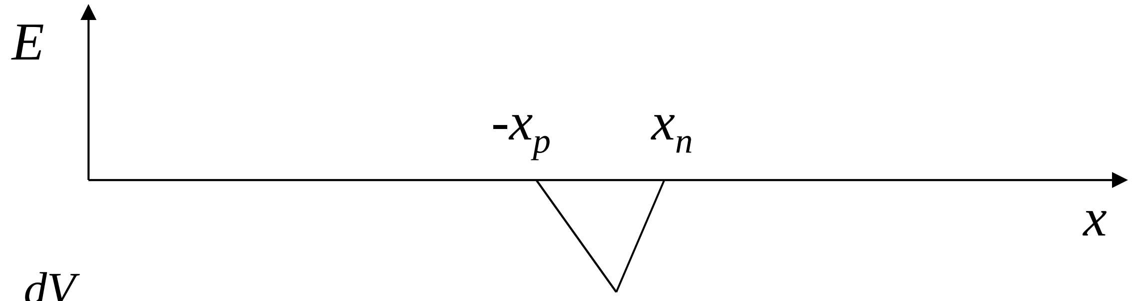
Oxide isolated integrated BJT - a modern process

abrupt junction



$$eV_{bi} = k_B T \ln\left(\frac{N_D N_A}{n_i^2}\right)$$

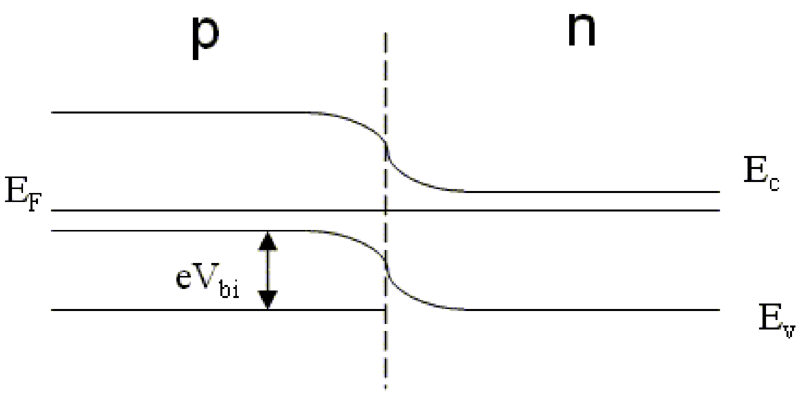
$$\frac{dE}{dx} = \frac{\rho}{\varepsilon}$$



$$E = -\frac{eN_A}{\varepsilon}\left(x + x_p\right) \qquad -x_p > x > 0$$

$$E = \frac{eN_D}{\varepsilon}\left(x - x_n\right) \qquad 0 > x > x_n$$

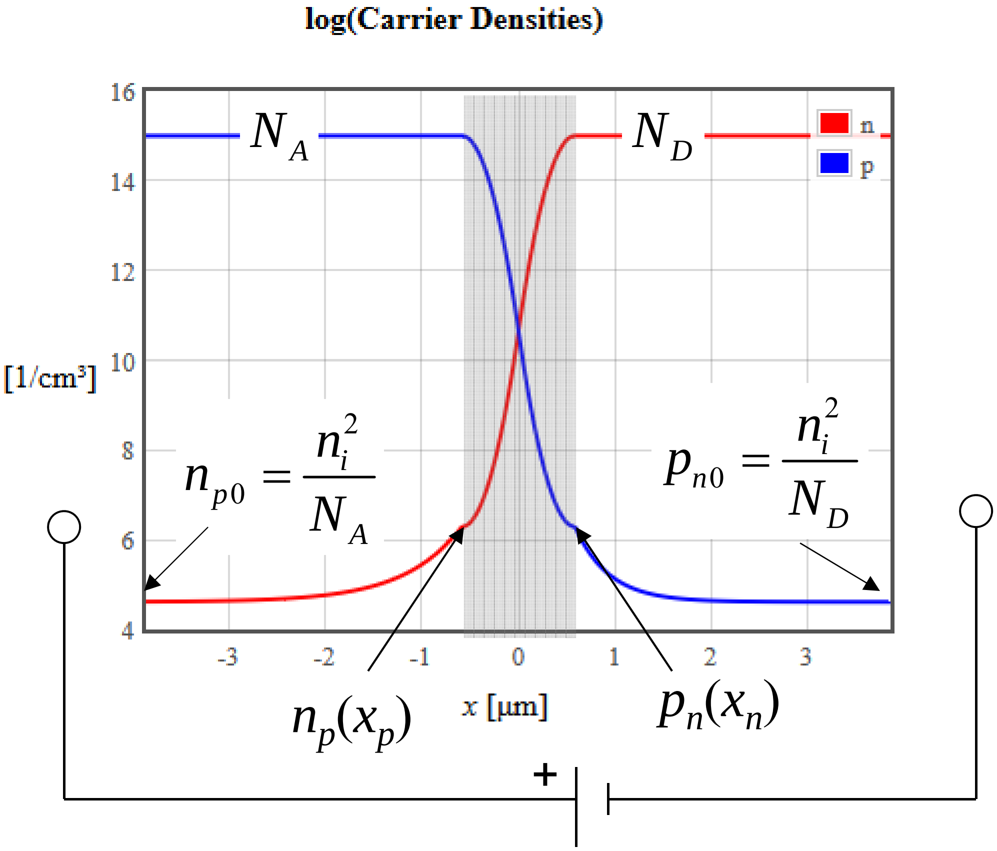
$$\frac{dV}{dx} = -E$$



$$V = \frac{eN_A}{\varepsilon}\left(\frac{x^2}{2} + xx_p\right) \qquad -x_p > x > 0$$

$$V = \frac{-eN_D}{\varepsilon}\left(\frac{x^2}{2} - xx_n\right) \qquad 0 > x > x_n$$

Forward bias, V > 0



Electrons and holes are driven towards the junction.
The depletion region becomes narrower

$$n_p(x_p) = N_D \exp\left(\frac{-e(V_{bi} - V)}{k_B T}\right)$$

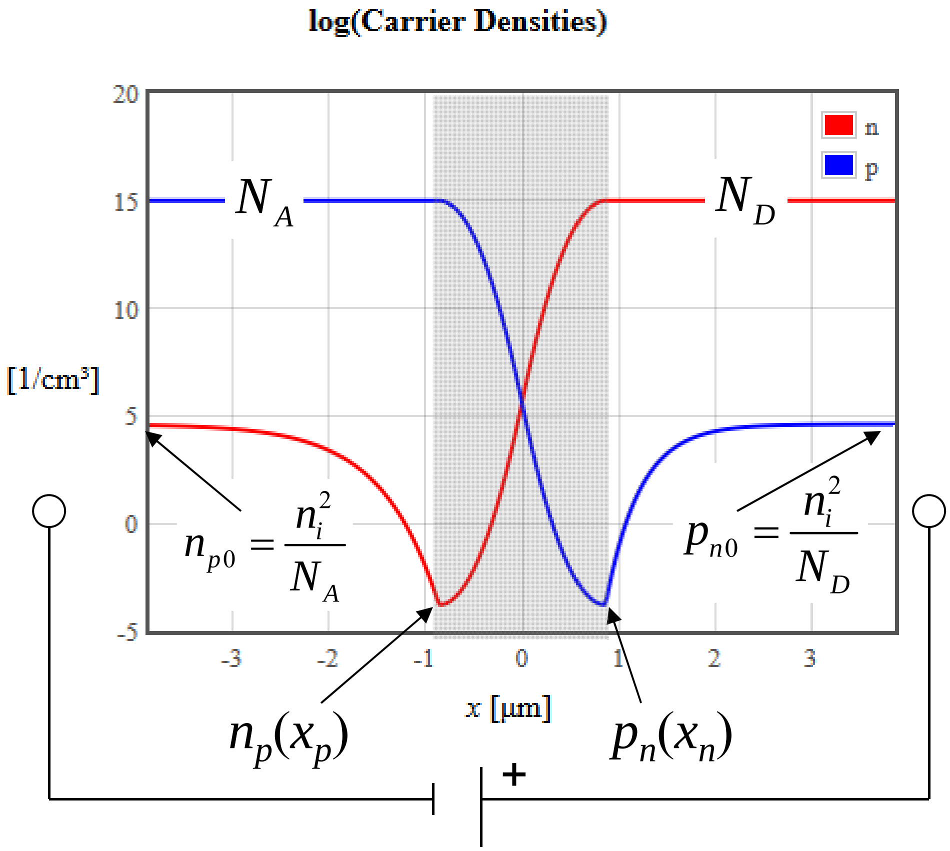
$$= n_{p0} \exp\left(\frac{eV}{k_B T}\right)$$

$$p_n(x_n) = N_A \exp\left(\frac{-e(V_{bi} - V)}{k_B T}\right)$$

$$= p_{n0} \exp\left(\frac{eV}{k_B T}\right)$$

Minority electrons are injected into the p-region
Minority holes are injected into the n-region

Reverse bias, V < 0



Electrons and holes are driven away from the junction.

The depletion region becomes wider

$$n_p(x_p) = N_D \exp\left(\frac{-e(V_{bi} - V)}{k_B T}\right)$$

$$= n_{p0} \exp\left(\frac{eV}{k_B T}\right)$$

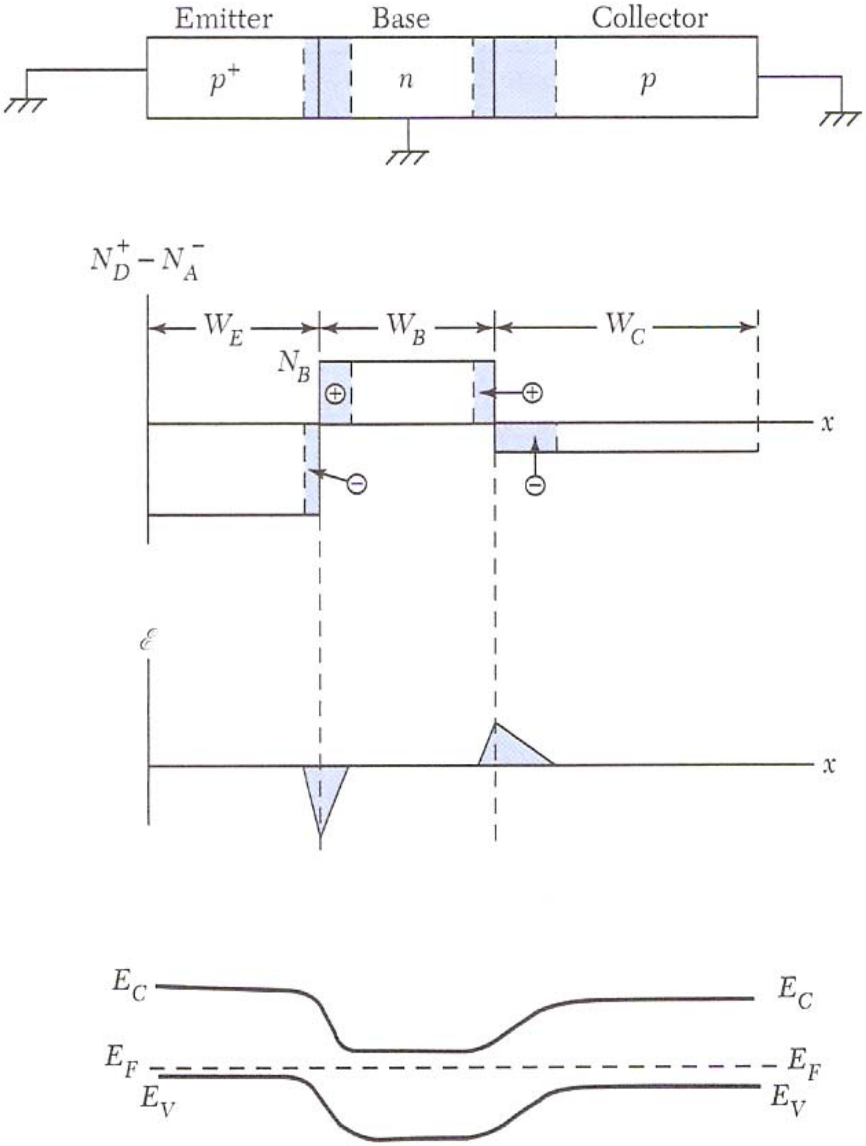
$$p_n(x_n) = N_A \exp\left(\frac{-e(V_{bi} - V)}{k_B T}\right)$$

$$= p_{n0} \exp\left(\frac{eV}{k_B T}\right)$$

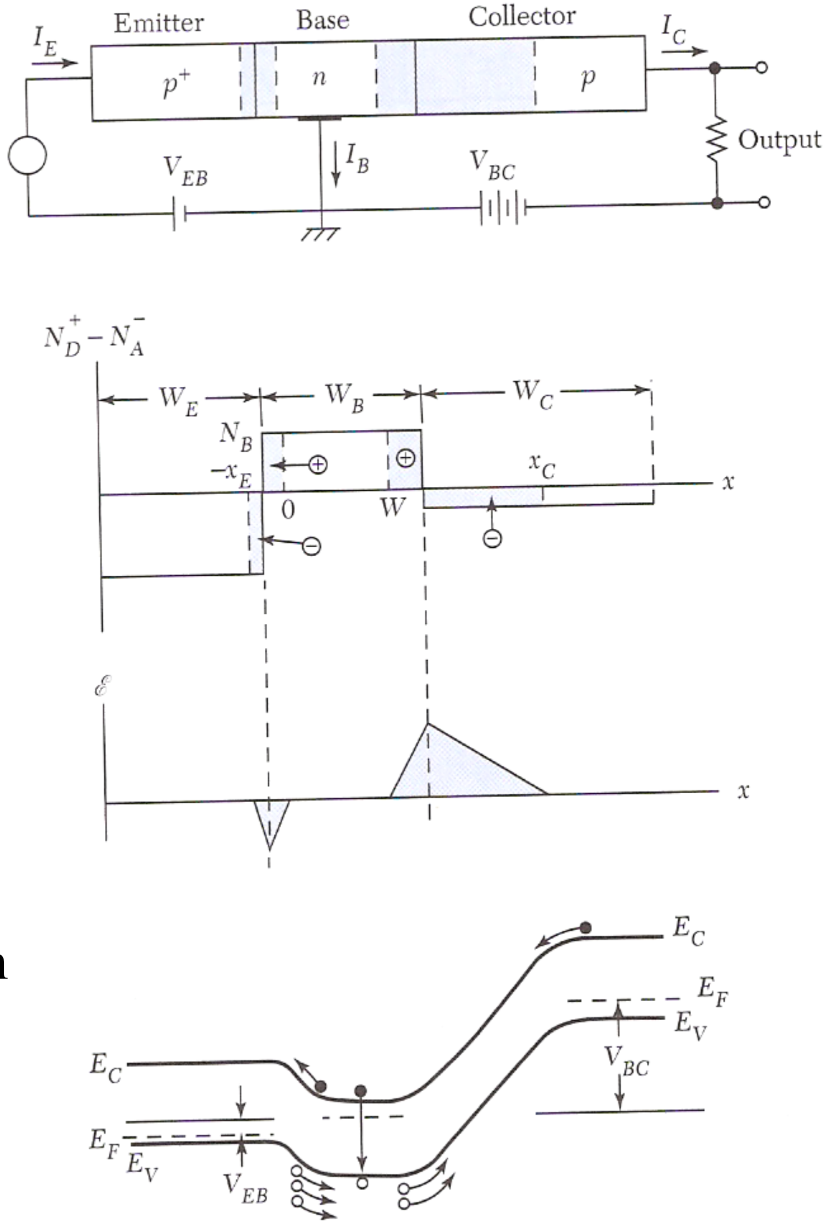
Minority electrons are extracted from the p-region by the electric field

Minority holes are extracted from the n-region by the electric field

pnp transistor, no bias



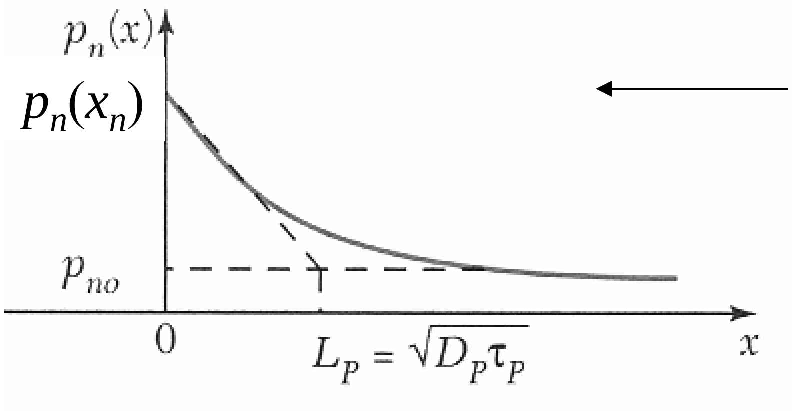
pnp transistor, forward active bias



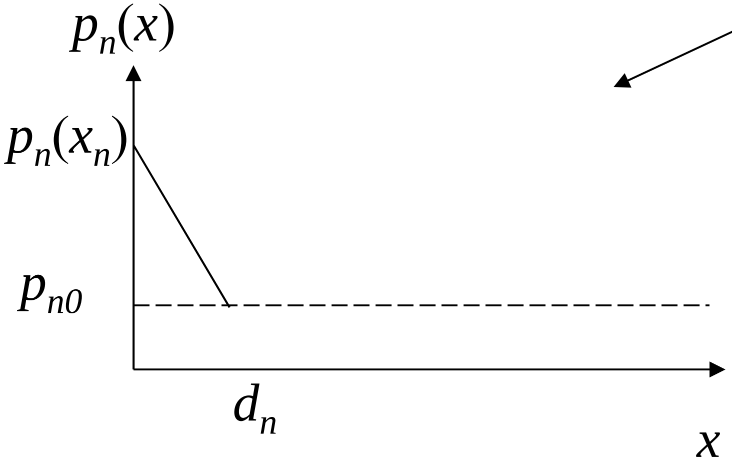
Always dissipate power due to the forward bias

The base-emitter voltage controls the minority carriers injected from the emitter to the base. These diffuse to the base-collector junction and are swept into the collector.

Long/Short diode



Long diode $d_n >> L_p$



Short diode

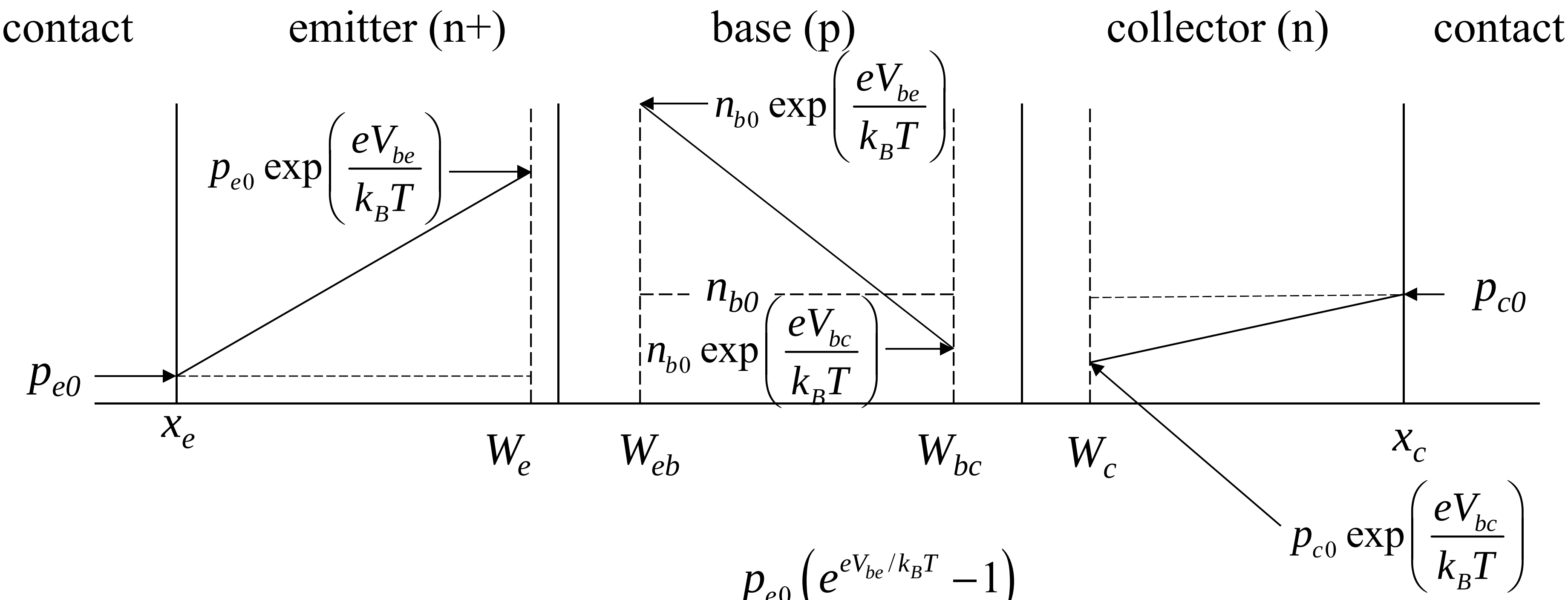
$d_n << L_p$

Metal contact is much closer to the depletion region than the diffusion length

$$J_{diff,p} = eD_p \frac{dp}{dx}$$

$$J_{diff,p} = eD_p \frac{dp}{dx} = eD_p \frac{\left(p_n(x_n) - p_{n0}\right)}{d_n}$$

Minority carrier concentration



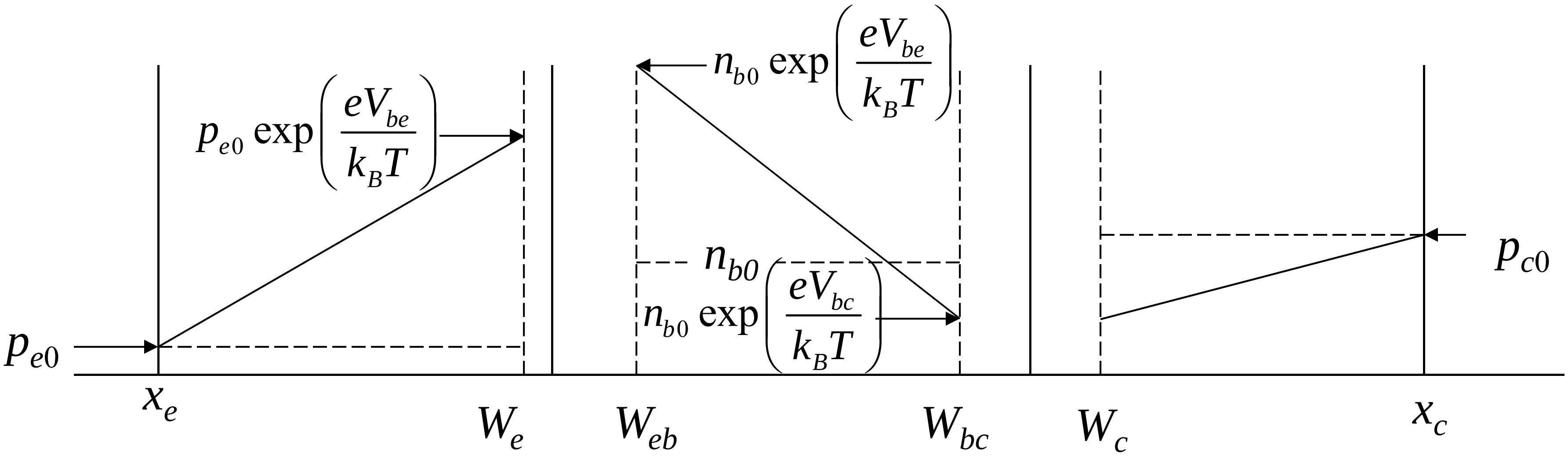
$$I_{Ep} = eA_{be}D_p \frac{p_{e0}\left(e^{eV_{be}/k_BT}-1\right)}{W_e - x_e}$$

$$I_{En} = -eA_{be}D_n \frac{n_{b0}\left(e^{eV_{be}/k_BT}-e^{eV_{bc}/k_BT}\right)}{W_{bc}-W_{be}}$$

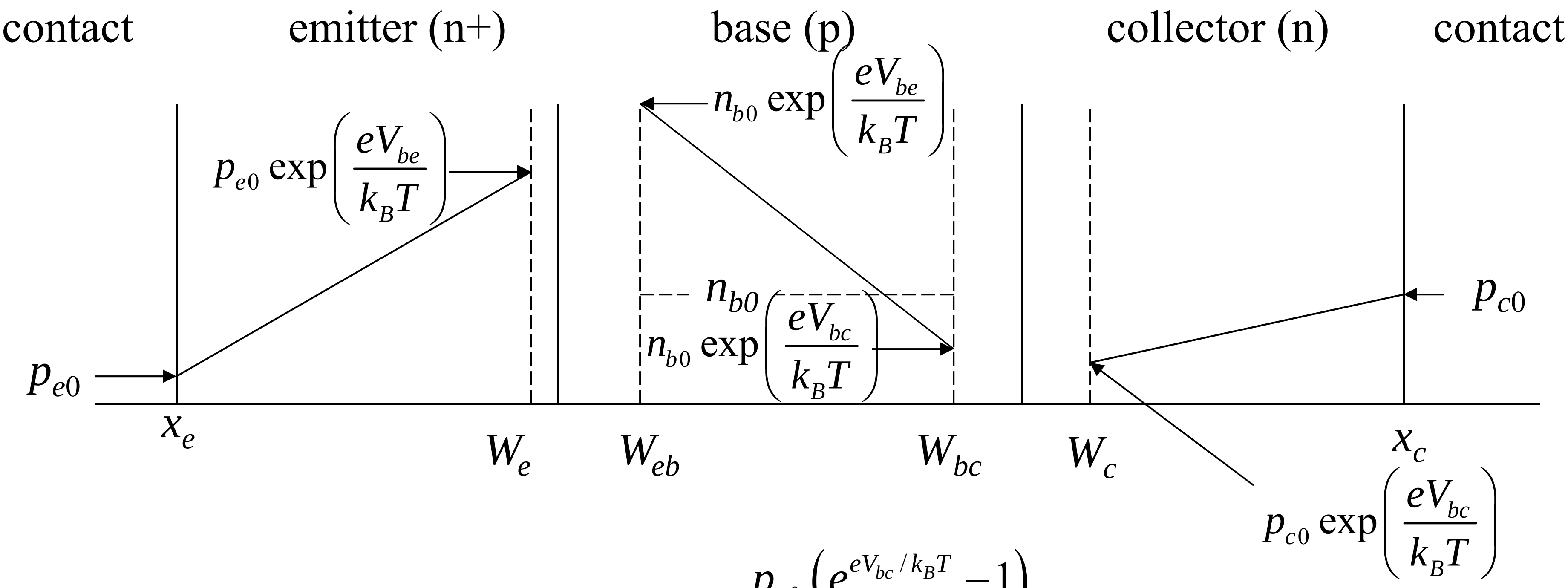
Emitter current

$$I_E = I_{En} + I_{Ep} = \left[\frac{eA_{be}D_p p_{e0}}{W_{eb} - x_e} + \frac{eA_{be}D_n n_{b0}}{W_{bc} - W_{be}}\right]\left(e^{eV_{be}/k_BT} - 1\right) - \frac{eA_{be}D_n n_{b0}}{W_{bc} - W_{be}}\left(e^{eV_{bc}/k_BT} - 1\right)$$

$$I_E = I_{ES}\left(e^{eV_{be}/k_BT} - 1\right) - \alpha_R I_{CS}\left(e^{eV_{bc}/k_BT} - 1\right)$$



Collector current



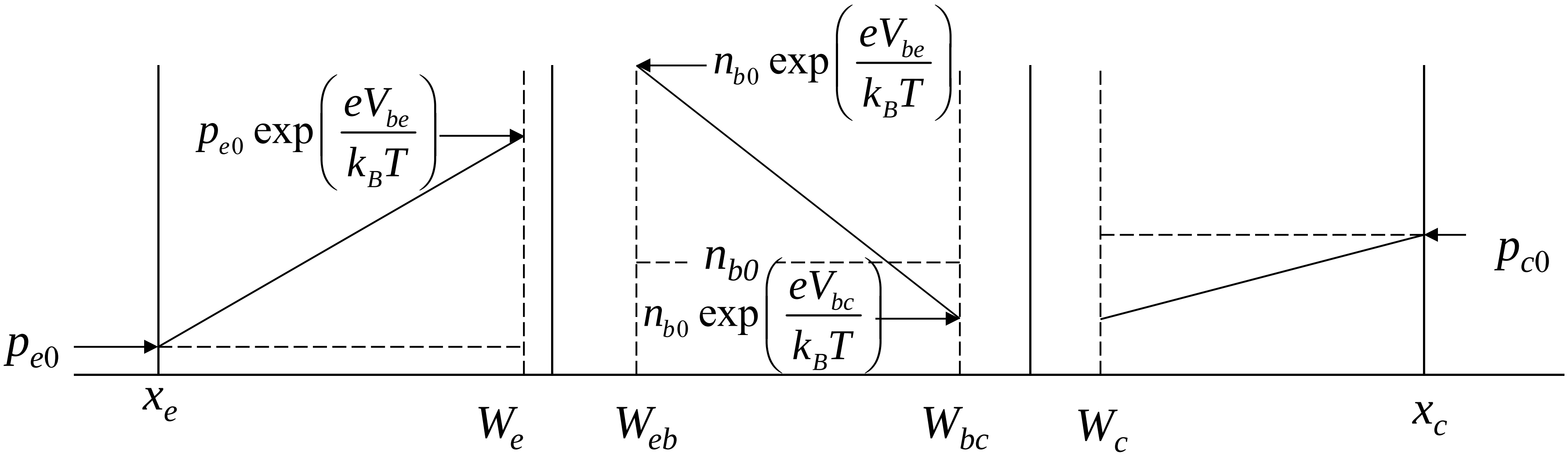
$$I_{cp} = -eA_{bc} D_p \frac{p_{c0}\left(e^{eV_{bc}/k_B T} - 1\right)}{x_c - W_c}$$

$$I_{cn} = -eA_{bc} D_n \frac{n_{b0}\left(e^{eV_{be}/k_B T} - e^{eV_{bc}/k_B T}\right)}{W_{bc} - W_{eb}}$$

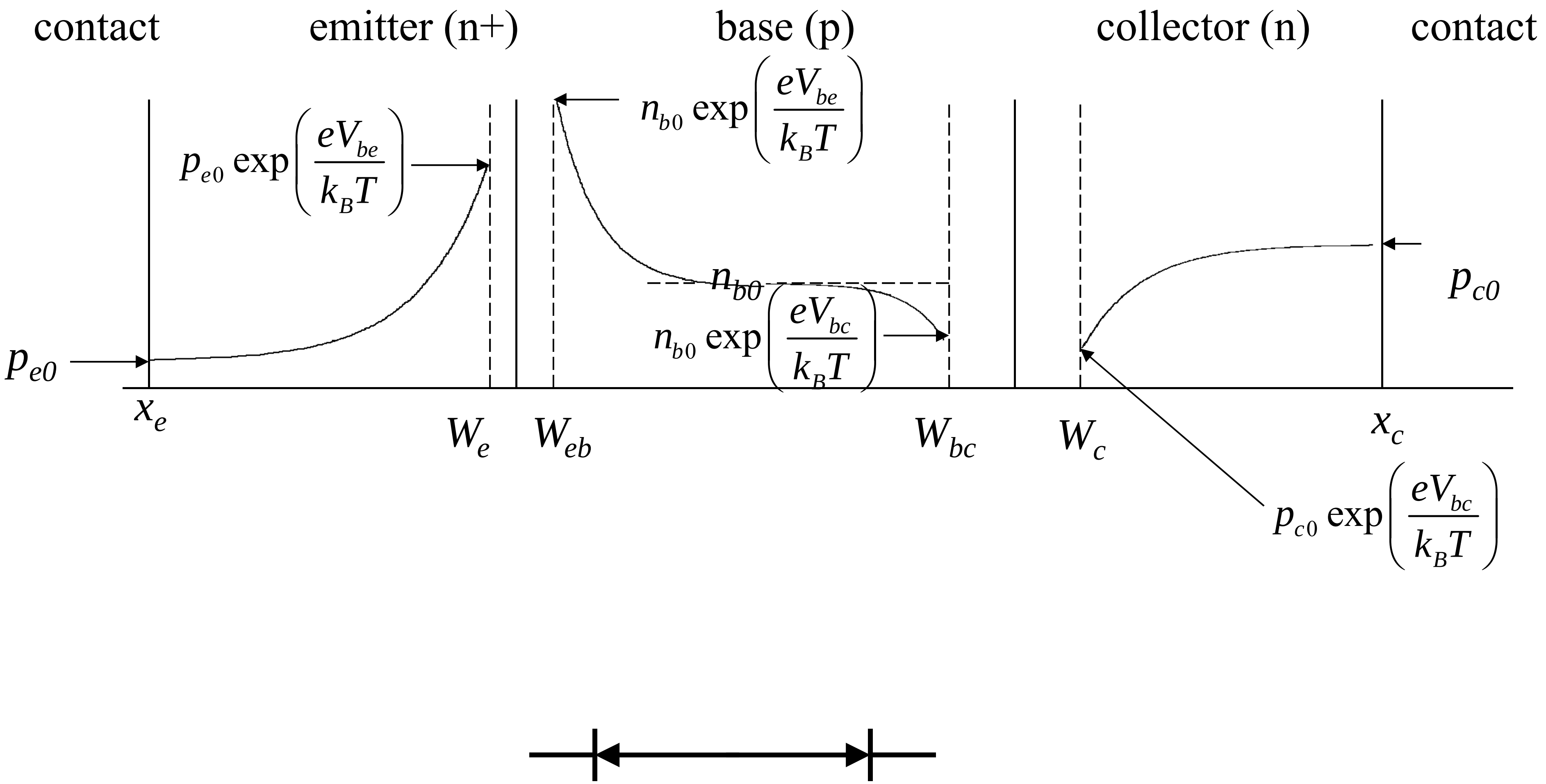
Collector current

$$I_c = I_{cp} + I_{cn} = \frac{eA_{bc}D_n n_{b0}}{W_{bc} - W_{be}}\left(e^{eV_{be}/k_BT} - 1\right) - \left[\frac{eA_{bc}D_p p_{c0}}{x_c - W_c} + \frac{eA_{bc}D_n n_{b0}}{W_{bc} - W_{be}}\right]\left(e^{eV_{bc}/k_BT} - 1\right)$$

$$I_c = I_{cp} + I_{cn} = \alpha_F I_{ES}\left(e^{eV_{be}/k_BT} - 1\right) - I_{CS}\left(e^{eV_{bc}/k_BT} - 1\right)$$



Not an npn transistor

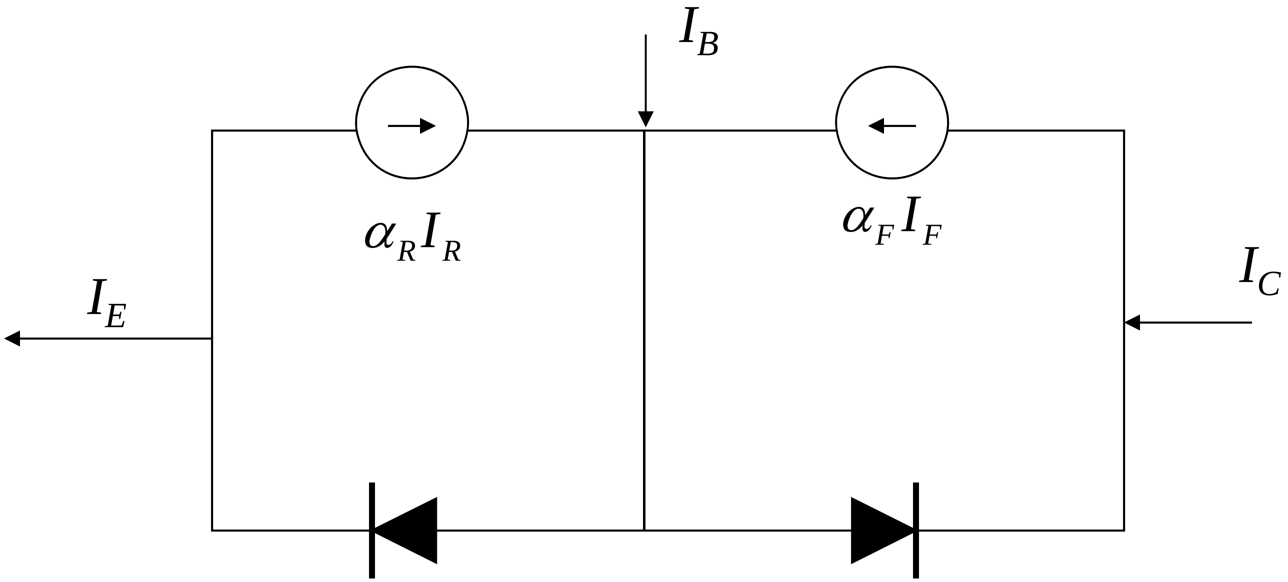


Ebers-Moll model

$$I_E = I_{ES}\left(e^{eV_{be}/k_BT}-1\right)-\alpha_R I_{CS}\left(e^{eV_{bc}/k_BT}-1\right)$$

$$I_C = \alpha_F I_{ES}\left(e^{eV_{be}/k_BT}-1\right)-I_{CS}\left(e^{eV_{bc}/k_BT}-1\right)$$

$$I_B = I_E - I_C$$



$$I_F = I_{ES}\left(e^{eV_{be}/k_BT}-1\right) \qquad I_R = I_{CS}\left(e^{eV_{bc}/k_BT}-1\right)$$

Emitter efficiency

$$\gamma_e = \frac{I_{En}}{I_{En} + I_{Ep}} = \frac{1}{1 + I_{Ep} / I_{En}}$$

for npn

$$I_{Ep} = eA_{be} D_p \frac{p_{e0}\left(e^{eV_{be}/k_B T} - 1\right)}{W_{eb} - x_e}$$

$$I_{En} = -eA_{be} D_n \frac{n_{b0}\left(e^{eV_{be}/k_B T} - e^{eV_{bc}/k_B T}\right)}{W_{bc} - W_{be}}$$

For $\gamma_e \sim 1$, $W_{bc} - W_{be} << L_b$, $W_{eb} - x_e$ and $n_{b0} >> p_{e0}$

neutral base width

$$\frac{n_i^2}{N_{Ab}}$$

$$\frac{n_i^2}{N_{De}}$$

Small base width and heavy emitter doping

Base transport factor

$$B = \frac{I_c}{I_{En}}$$

ratio of the injected current to the collected current

recombination in the base would reduce the base transport factor

A thin base with low doping results in a base transport factor ~ 1

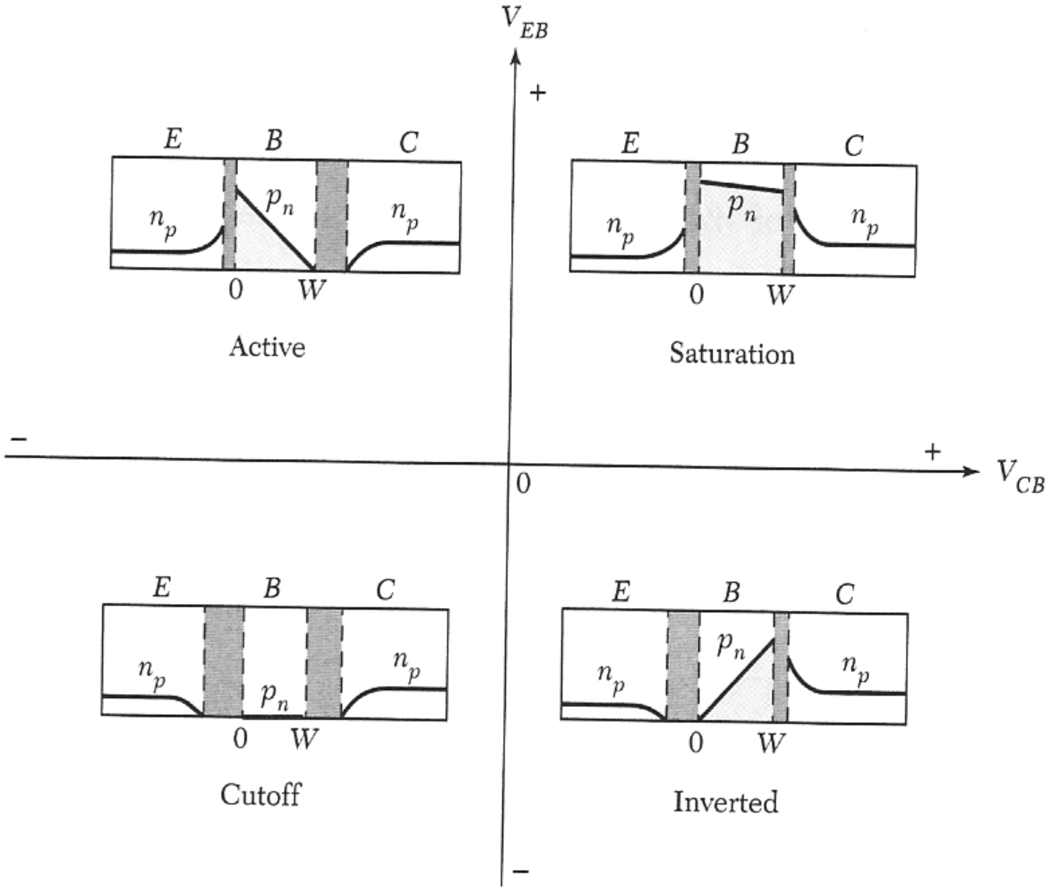
Current transfer ratio

$$\alpha = \frac{I_C}{I_E} = B\gamma_e$$

$\alpha \sim 1$ for a good BJT

Transistor modes

1. Forward active: emitter-base **forward**, base-collector **reverse**
2. Saturation: emitter-base **forward**, base-collector **forward**
3. Reverse active: emitter-base **reverse**, base-collector **forward**
4. Cut-off: emitter-base **reverse**, base-collector **reverse**

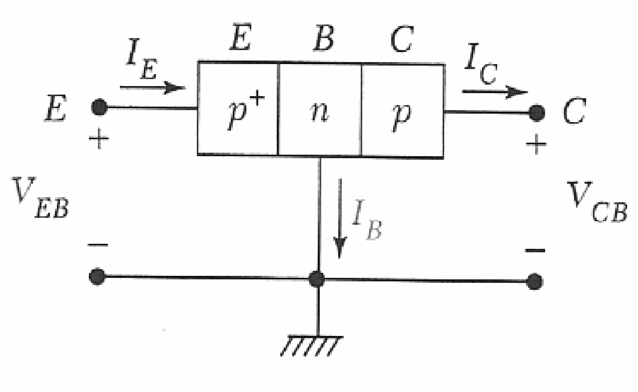


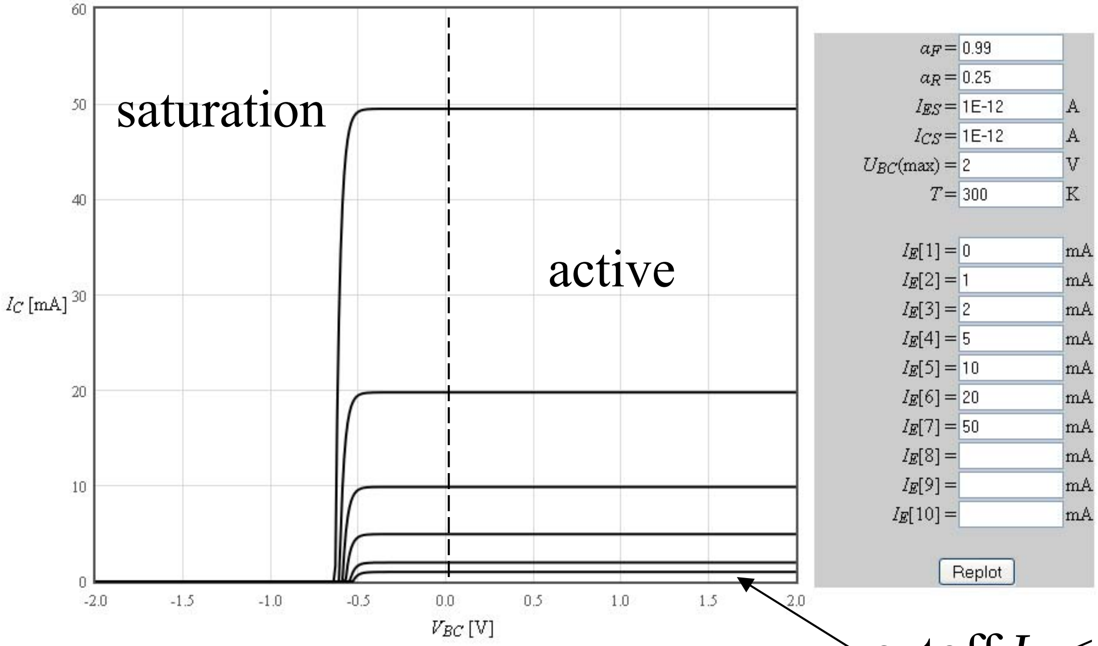
Common base configuration

$$I_E = I_{ES}\left(e^{eV_{be}/k_BT} - 1\right) - \alpha_R I_{CS}\left(e^{eV_{bc}/k_BT} - 1\right)$$

solve for V_{be}

$$I_c = \alpha_F I_{ES}\left(e^{eV_{be}/k_BT} - 1\right) - I_{CS}\left(e^{eV_{bc}/k_BT} - 1\right)$$





saturation

active

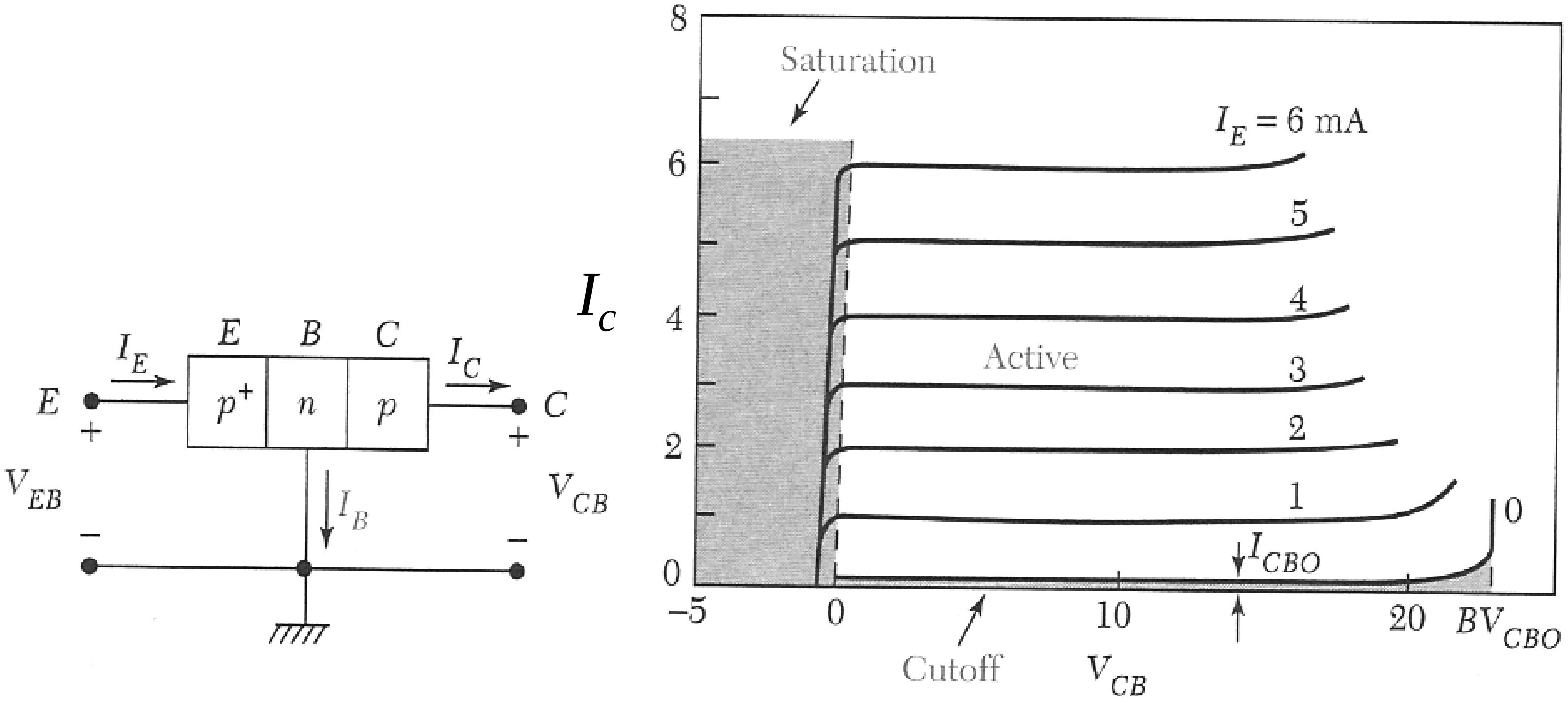
$\alpha_F =$ 0.99
$\alpha_R =$ 0.25
$I_{ES} =$ 1E-12 A
$I_{CS} =$ 1E-12 A
U_{BC}(max) = 2 V
$T =$ 300 K

$I_E[1] =$ 0 mA
$I_E[2] =$ 1 mA
$I_E[3] =$ 2 mA
$I_E[4] =$ 5 mA
$I_E[5] =$ 10 mA
$I_E[6] =$ 20 mA
$I_E[7] =$ 50 mA
$I_E[8] =$ mA
$I_E[9] =$ mA
$I_E[10] =$ mA

cutoff $I_E < 0$

http://lamp.tu-graz.ac.at/~hadley/psd/L13/commonbase/pnp_current.html

Common base configuration



$I_C \sim I_E$ buffer circuit: the output current is constant over a wide range of output voltages

Ebers - Moll Model

$$I_{ES} = \left[\frac{eA_{be} D_p p_{e0}}{W_{eb} - x_e} + \frac{eA_{be} D_n n_{b0}}{W_{bc} - W_{be}} \right]$$

$$\alpha_R I_{CS} = \frac{eA_{be} D_n n_{b0}}{W_{bc} - W_{be}}$$

$$\alpha_F I_{ES} = \frac{eA_{bc} D_n n_{b0}}{W_{bc} - W_{be}}$$

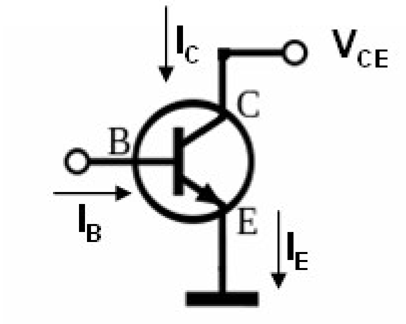
$$I_{CS} = \left[\frac{eA_{bc} D_p p_{c0}}{x_c - W_c} + \frac{eA_{bc} D_n n_{b0}}{W_{bc} - W_{be}} \right]$$

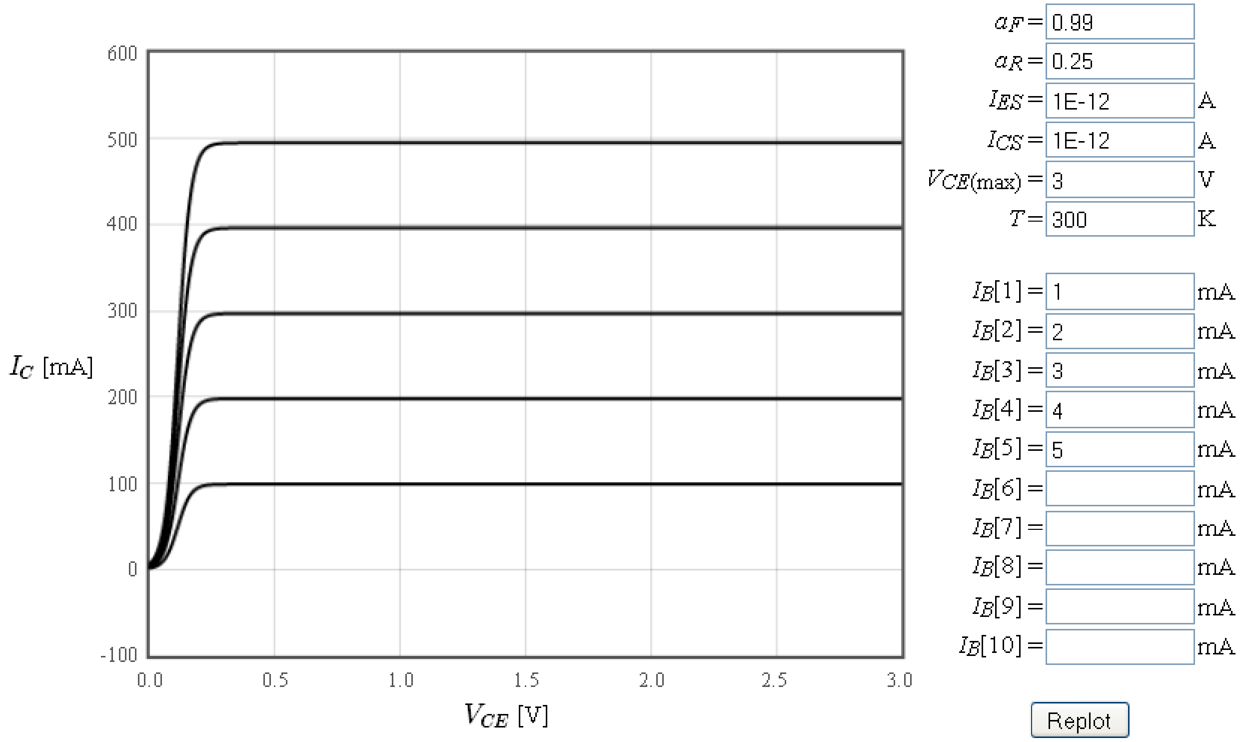
Common emitter configuration

$$I_E = I_{ES}\left(e^{eV_{be}/k_BT}-1\right)-\alpha_R I_{CS}\left(e^{eV_{bc}/k_BT}-1\right)$$

$$I_B = I_E - I_C$$

$$I_c = \alpha_F I_{ES}\left(e^{eV_{be}/k_BT}-1\right)-I_{CS}\left(e^{eV_{bc}/k_BT}-1\right)$$





α_F = 0.99
α_R = 0.25
I_{ES} = 1E-12 A
I_{CS} = 1E-12 A
V_{CE}(max) = 3 V
T = 300 K

$I_B[1]$ = 1 mA
$I_B[2]$ = 2 mA
$I_B[3]$ = 3 mA
$I_B[4]$ = 4 mA
$I_B[5]$ = 5 mA
$I_B[6]$ = mA
$I_B[7]$ = mA
$I_B[8]$ = mA
$I_B[9]$ = mA
$I_B[10]$ = mA

current amplification ~100

http://lamp.tu-graz.ac.at/~hadley/psd/L13/commonemitter.php

Current amplification factor

$$\beta = h_{fe} = \frac{I_C}{I_B}$$

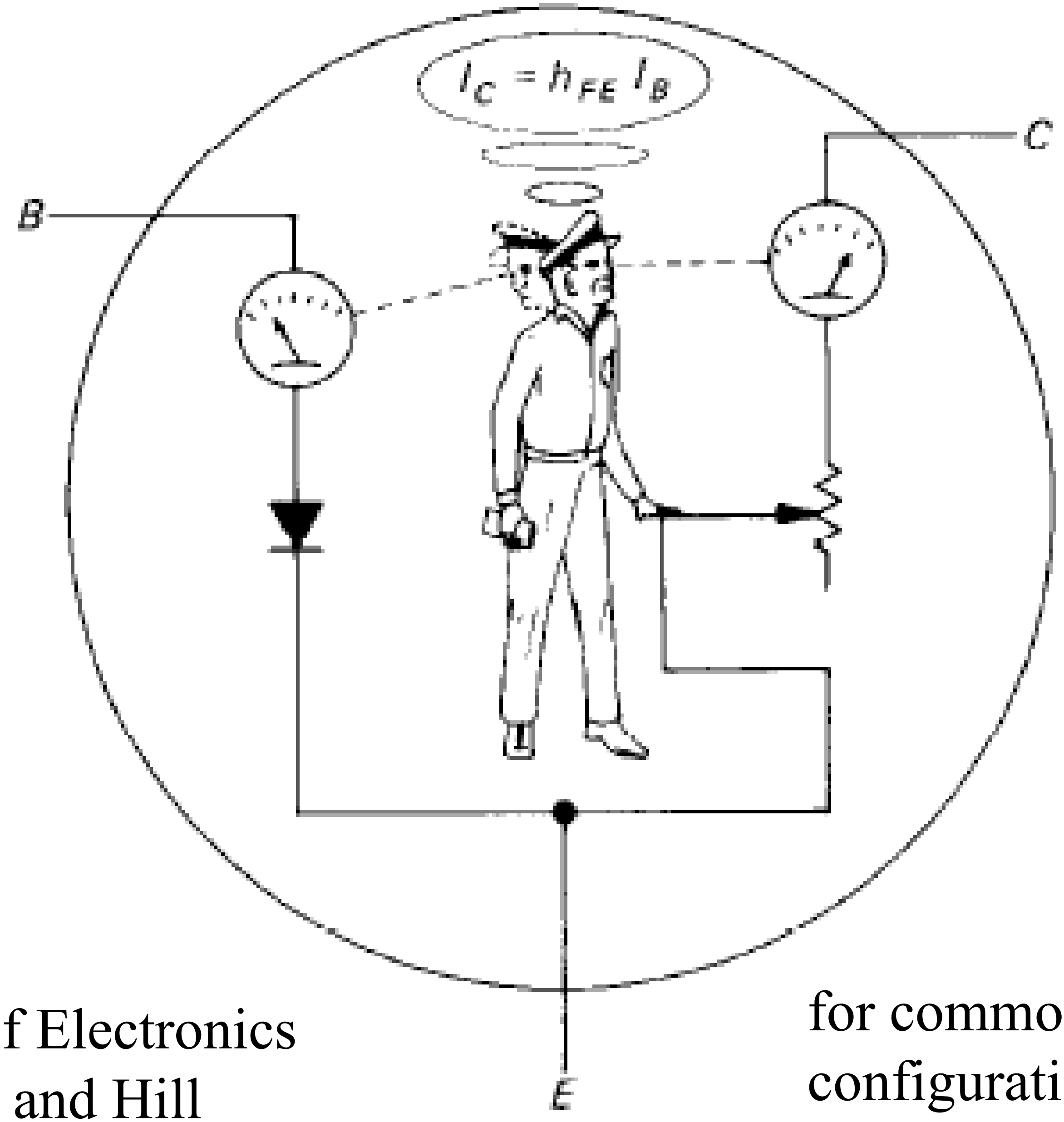
$$I_B = I_E - I_C$$

$$I_C = \alpha I_E$$

$$I_B = \left(\frac{1}{\alpha} - 1 \right) I_C$$

$$\beta = \frac{I_C}{I_B} = \frac{\alpha}{1-\alpha} = \frac{B\gamma_e}{1 - B\gamma_e}$$

$\beta \sim 50 - 500$



The Art of Electronics
Horowitz and Hill

for common emitter
configuration

“Transistor man”

Transconductance

$$g_m = \frac{\partial I_C}{\partial V_{be}}$$

$$I_c = \alpha_F I_{ES}\left(e^{eV_{be}/k_BT} - 1\right) - I_{CS}\left(e^{eV_{bc}/k_BT} - 1\right)$$

The first term depends on V_{be}

$$g_m = \frac{e\alpha_F I_{ES}}{k_BT} e^{eV_{be}/k_BT} \approx \frac{eI_C}{k_BT} = \frac{e\beta I_B}{k_BT}$$

The transconductance can be very high.

Early effect

Ebers - Moll:

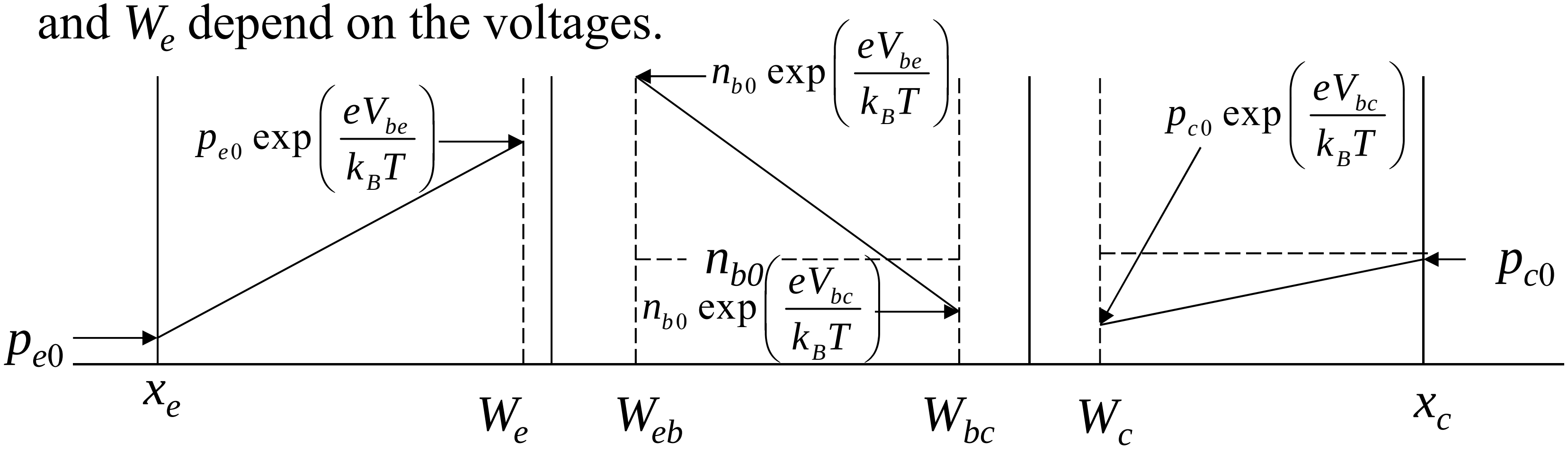
$$I_E = I_{ES}\left(e^{eV_{be}/k_BT} - 1\right) - \alpha_R I_{CS}\left(e^{eV_{bc}/k_BT} - 1\right)$$

$$I_c = \alpha_F I_{ES}\left(e^{eV_{be}/k_BT} - 1\right) - I_{CS}\left(e^{eV_{bc}/k_BT} - 1\right)$$

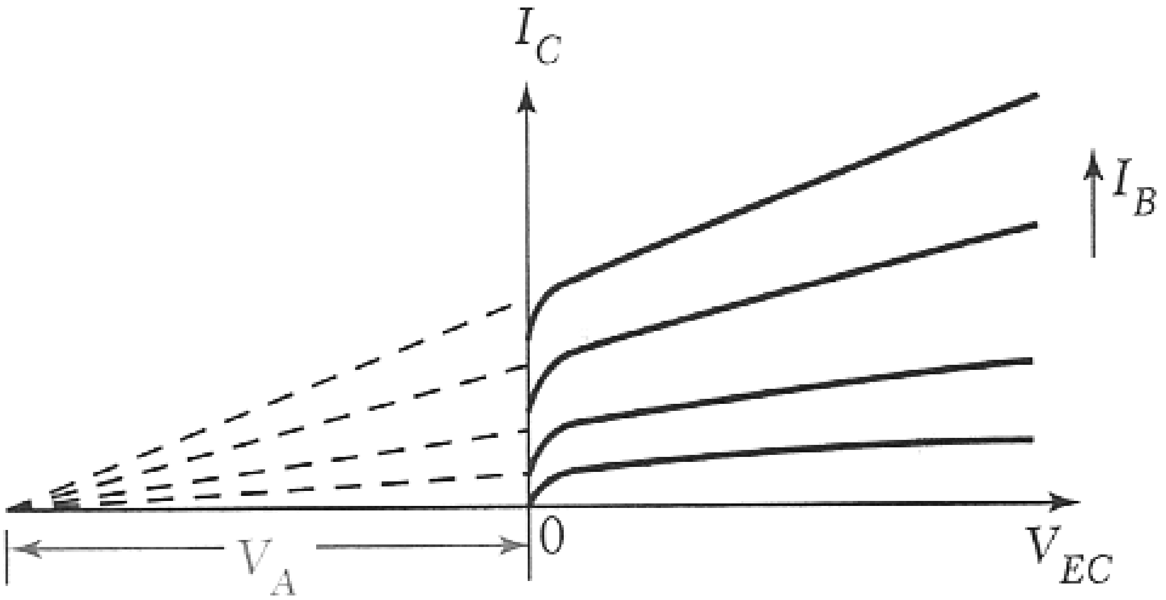
$$I_B = I_E - I_C$$

$$I_{ES} = \left[\frac{eA_{be}D_p p_{e0}}{W_{eb} - x_e} + \frac{eA_{be}D_n n_{b0}}{W_{bc} - W_{be}}\right] \qquad I_{CS} = \left[\frac{eA_{bc}D_p p_{c0}}{x_c - W_c} + \frac{eA_{bc}D_n n_{b0}}{W_{bc} - W_{be}}\right]$$

I_{ES} and I_{CS} are treated as constants but the depletion widths W_{bc}, W_{be}, W_c, and W_e depend on the voltages.



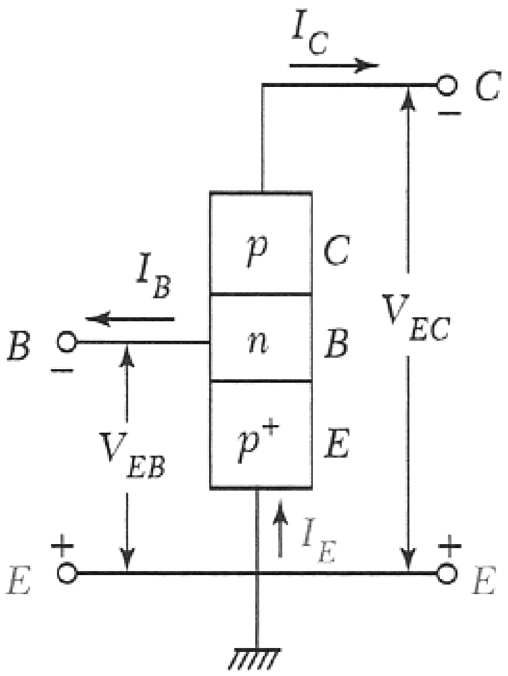
Early effect

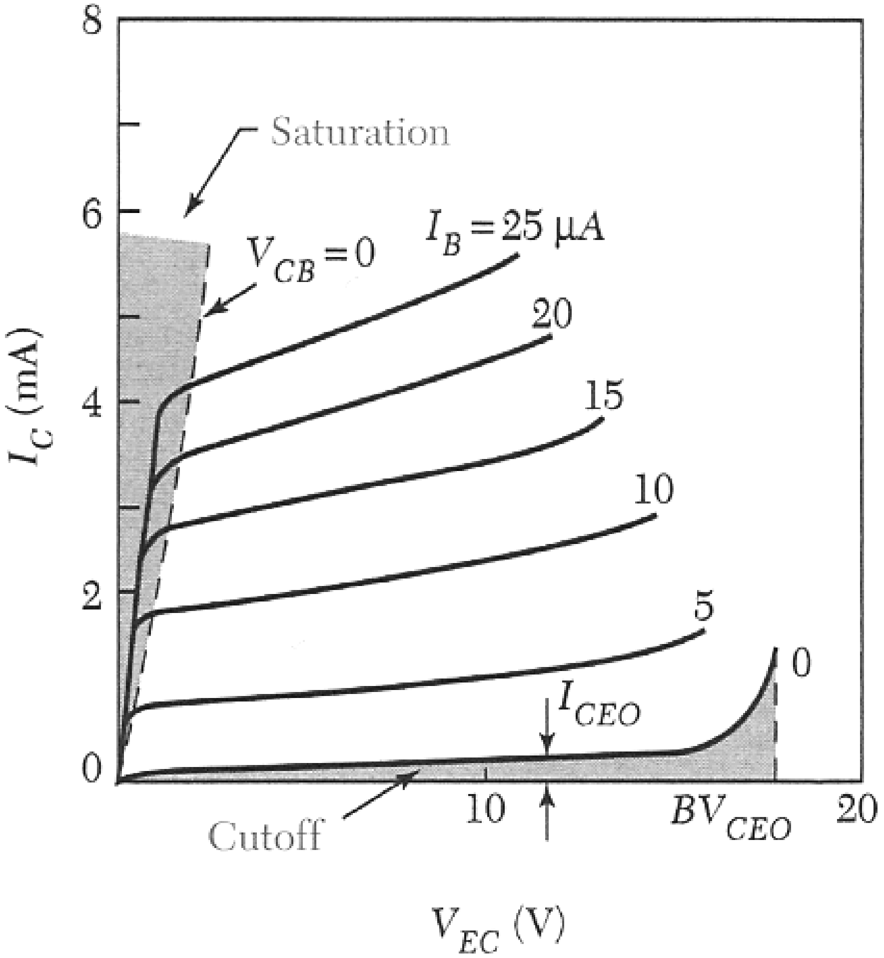


Common emitter configuration
Base width modulation: smaller width increases the diffusion current and increases the gain.

Punchthrough: The neutral base width goes to zero and all gain is lost.
Lightly dope the collector -> voltage drops in collector. Makes circuit slower.

Common emitter configuration





$I_C \sim \beta I_B$ amplifier