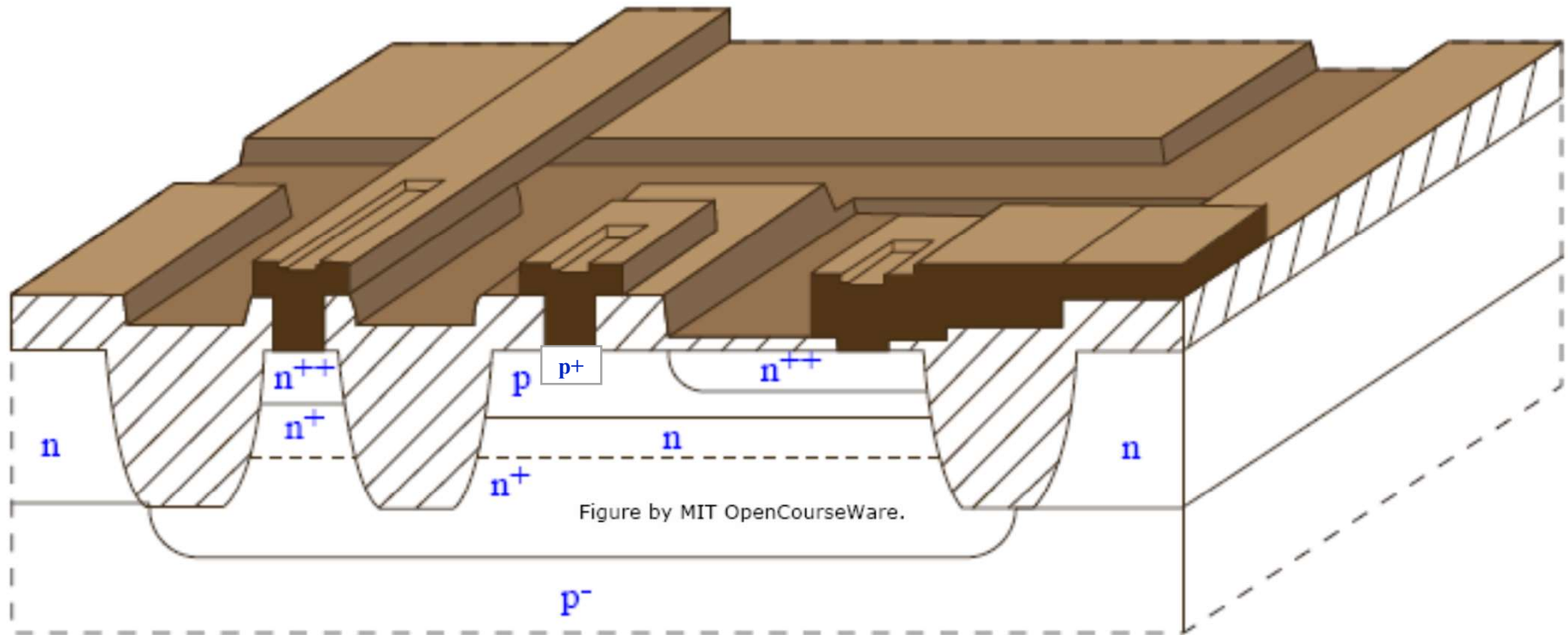
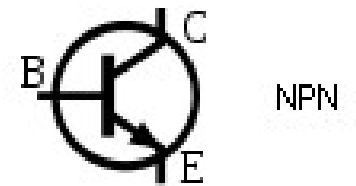
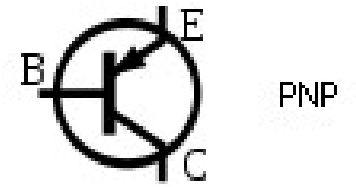


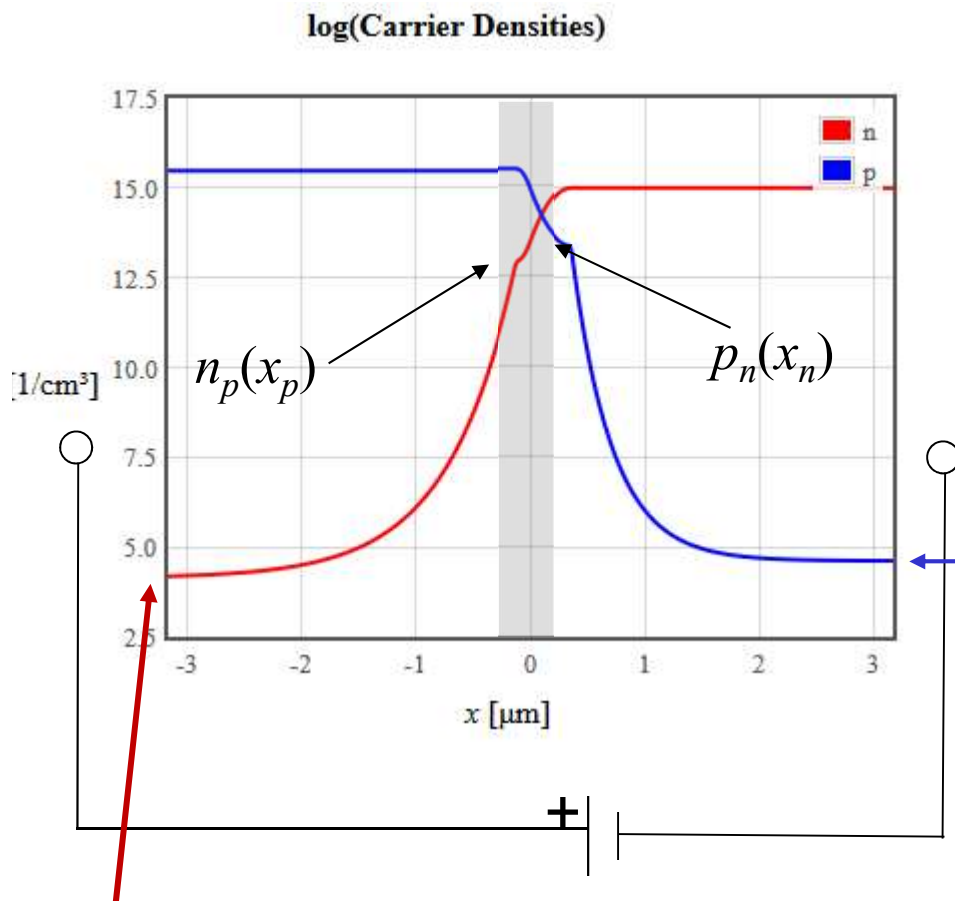
Bipolar transistors, Thyristors, and Latch-up

bipolar transistors



Oxide isolated integrated BJT - a modern process

Forward bias, $V > 0$



Electrons and holes are driven towards the junction.
The depletion region becomes narrower

$$n_p(x_p) = n_{p0} \exp\left(\frac{eV}{k_B T}\right)$$

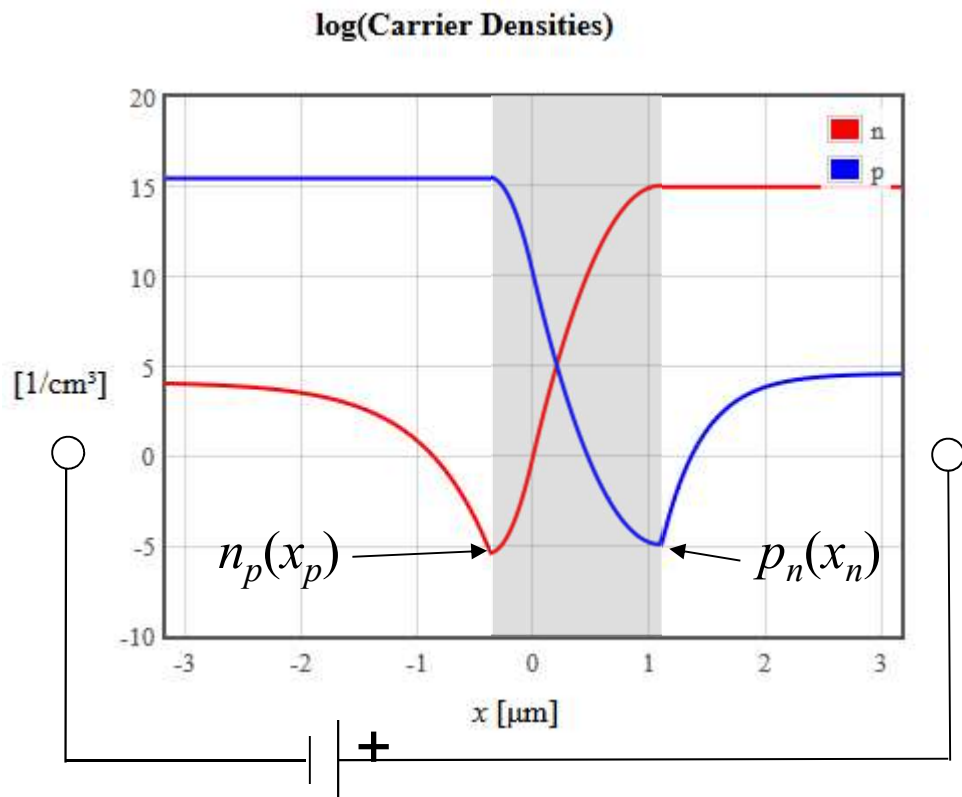
$$p_n(x_n) = p_{n0} \exp\left(\frac{eV}{k_B T}\right)$$

$$p_{n0} = \frac{n_i^2}{N_D}$$

$$n_{p0} = \frac{n_i^2}{N_A}$$

Minority electrons are injected into the p-region
Minority holes are injected into the n-region

Reverse bias, $V < 0$



Electrons and holes are driven away from the junction.

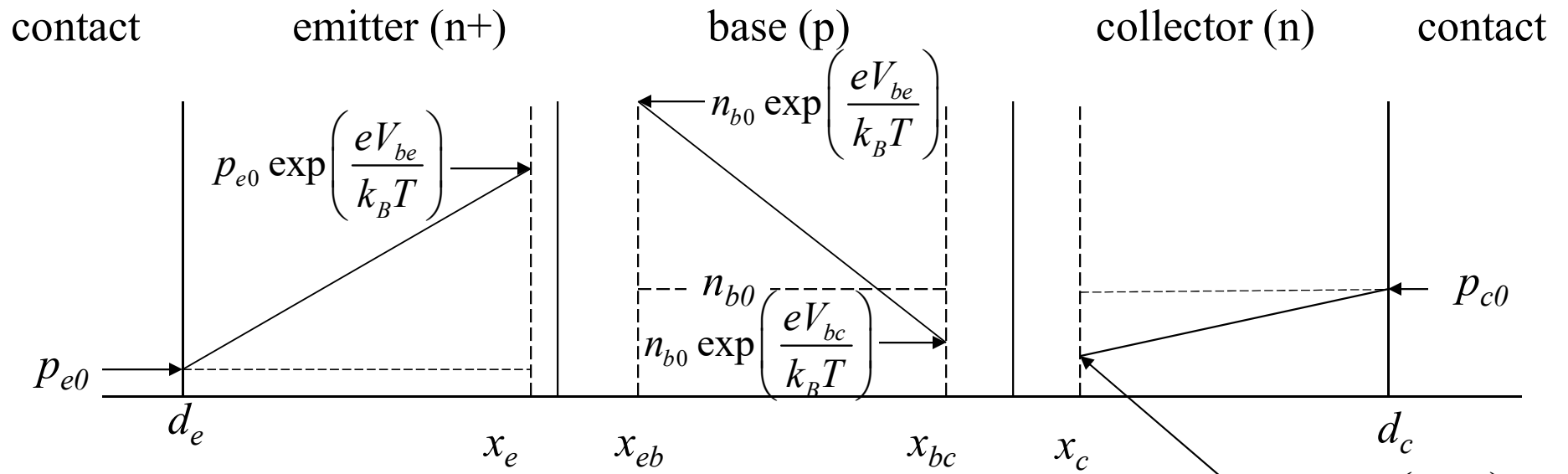
The depletion region becomes wider

$$n_p(x_p) = n_{p0} \exp\left(\frac{eV}{k_B T}\right)$$

$$p_n(x_n) = p_{n0} \exp\left(\frac{eV}{k_B T}\right)$$

Minority electrons are extracted from the p-region by the electric field
Minority holes are extracted from the n-region by the electric field

Minority carrier concentration



$$I_{Ep} = -eA_{be}D_p \frac{p_{e0}(e^{eV_{be}/k_B T} - 1)}{x_e - d_e}$$

$$I_{En} = eA_{be}D_n \frac{n_{b0}(e^{eV_{bc}/k_B T} - e^{eV_{be}/k_B T})}{x_{bc} - x_{be}}$$

Emitter efficiency

$$\gamma_e = \frac{I_{En}}{I_{En} + I_{Ep}} = \frac{1}{1 + I_{Ep} / I_{En}} \quad \leftarrow \text{for npn}$$

$$I_{Ep} = eA_{be}D_p \frac{p_{e0}(e^{eV_{be}/k_B T} - 1)}{x_{eb} - d_e}$$

$$I_{En} = -eA_{be}D_n \frac{n_{b0}(e^{eV_{be}/k_B T} - e^{eV_{bc}/k_B T})}{x_{bc} - x_{be}}$$

For $\gamma_e \sim 1$, $x_{bc} - x_{be} \ll L_b$, $x_{eb} - d_e$ and $n_{b0} \gg p_{e0}$

neutral base width

$$\frac{n_i^2}{N_{Ab}}$$

$$\frac{n_i^2}{N_{De}}$$

Small base width and heavy emitter doping

Base transport factor

$$B = \frac{I_c}{I_{En}}$$

ratio of the injected current to the collected current

recombination in the base would reduce the base transport factor

A thin base with low doping results in a base transport factor ~ 1

Early effect

Ebers - Moll:

$$I_E = I_{ES} \left(e^{eV_{be}/k_B T} - 1 \right) - \alpha_R I_{CS} \left(e^{eV_{bc}/k_B T} - 1 \right)$$

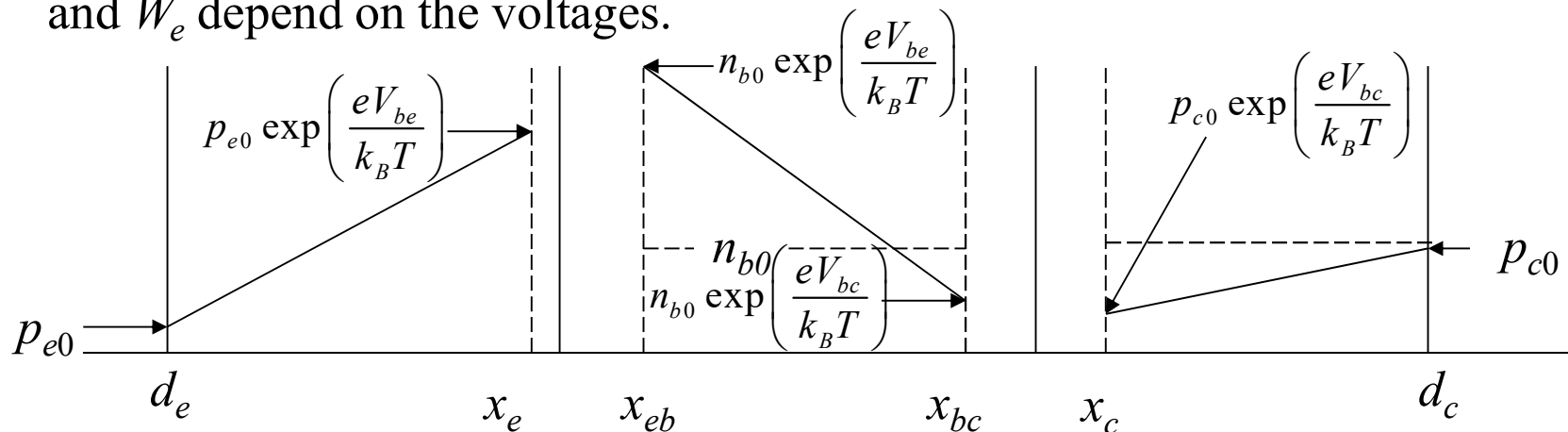
$$I_C = \alpha_F I_{ES} \left(e^{eV_{be}/k_B T} - 1 \right) - I_{CS} \left(e^{eV_{bc}/k_B T} - 1 \right)$$

$$I_B = I_E - I_C$$

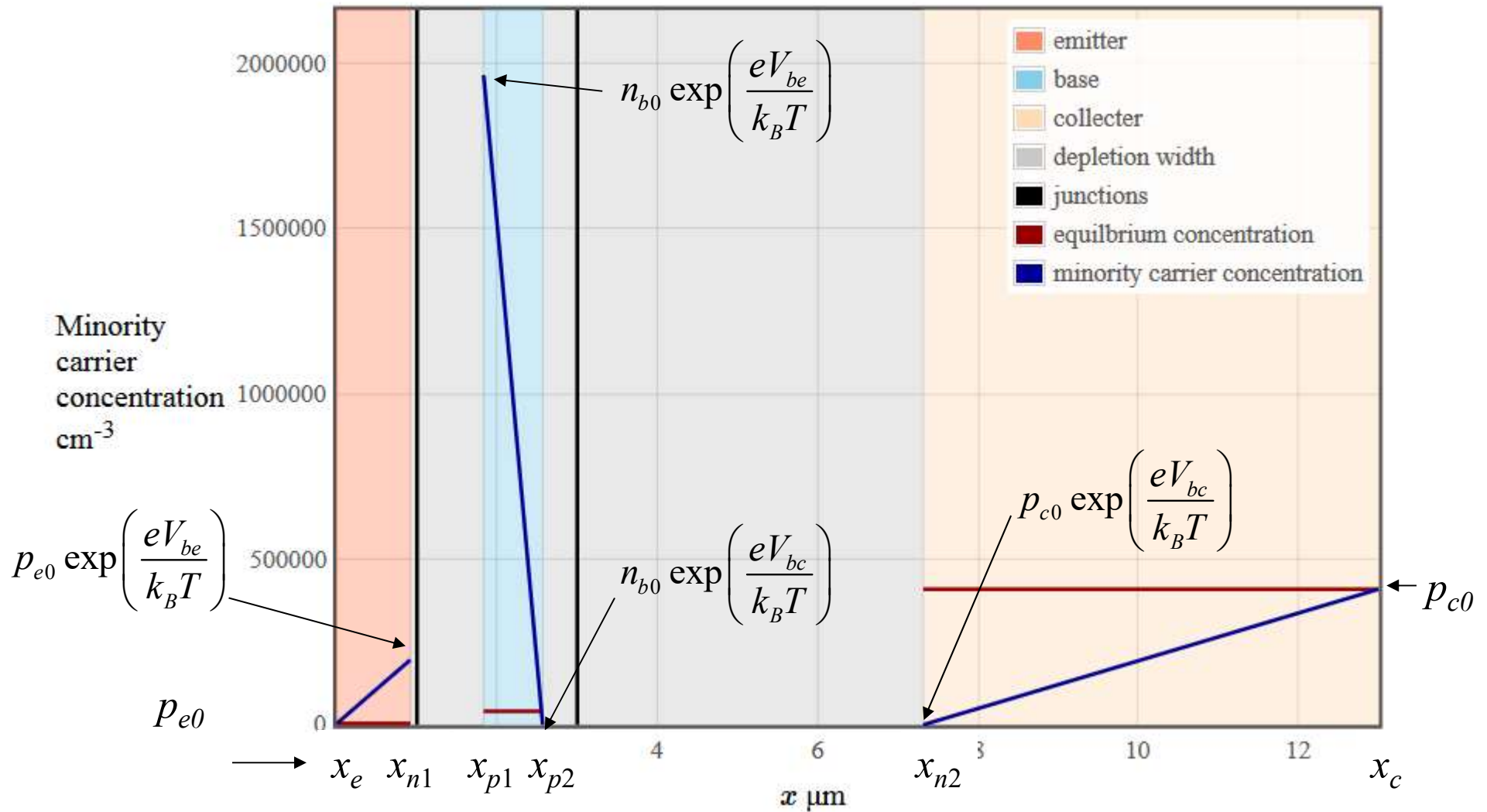
$$I_{ES} = \left[\frac{eA_{be}D_p p_{e0}}{x_{eb} - d_e} + \frac{eA_{be}D_n n_{b0}}{x_{bc} - x_{be}} \right]$$

$$I_{CS} = \left[\frac{eA_{bc}D_p p_{c0}}{d_c - x_c} + \frac{eA_{bc}D_n n_{b0}}{x_{bc} - x_{be}} \right]$$

I_{ES} and I_{CS} are treated as constants but the depletion widths W_{bc} , W_{be} , W_c and W_e depend on the voltages.



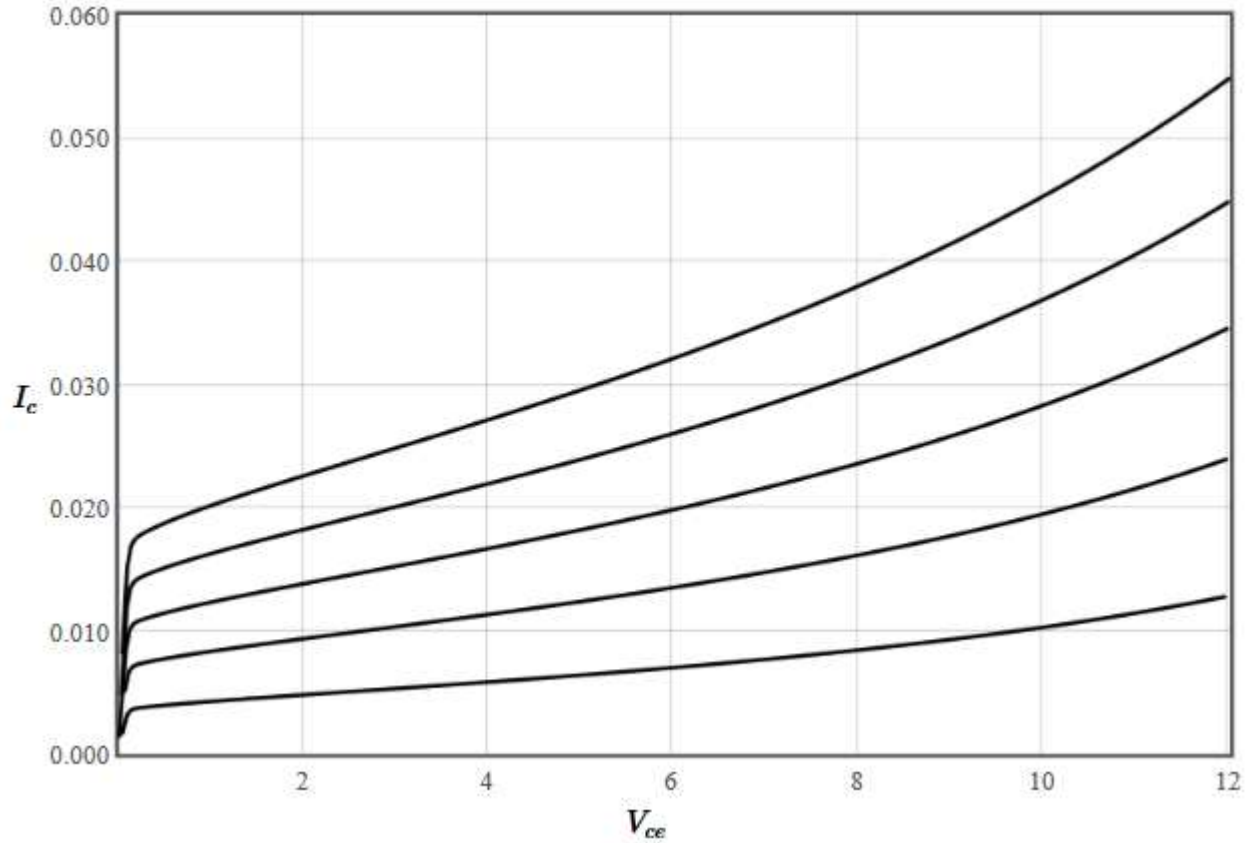
Minority carrier concentration



NPN common emitter configuration

n-Emitter		$A_{cb} = 1E-3$ cm ²
Minority $\mu_{pe} = 480$ cm ² /Vs	$N_{dc} = 1E16$ cm ⁻³	$N_c(300K) = 2.78E19$ cm ⁻³
$\tau_{pe} = 1E-5$ s		$N_v(300K) = 9.84E18$ cm ⁻³
		$E_g = 1.166-4.73E-4*T*(T+636)$ eV
		$\epsilon_r = 11.9$
p-Base		$I_{b,max} = 0.001$ eV
Minority $\mu_{nb} = 1350$ cm ² /Vs	$N_{cb} = 1E15$ cm ⁻³	$V_{ce,max} = 12$ eV
$\tau_{nb} = 1E-5$ s		$x_1 - x_e = 1$ μm
		$x_2 - x_1 = 2$ μm
		$x_c - x_2 = 10$ μm
		$T = 300$ K
n-Collector		
Minority $\mu_{pc} = 480$ cm ² /Vs	$N_{dc} = 1E14$ cm ⁻³	
$\tau_{pc} = 1E-5$ s		
<input type="button" value="Calculate"/>		

$$I_C \sim \beta I_B$$



Small signal response

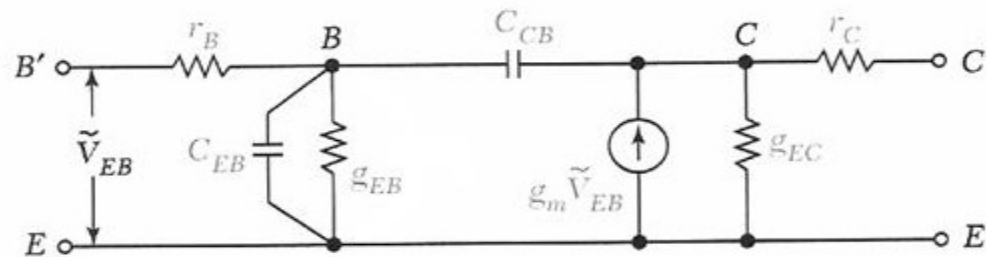
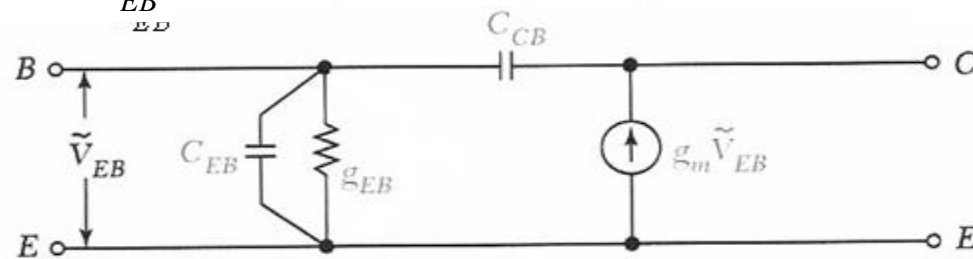
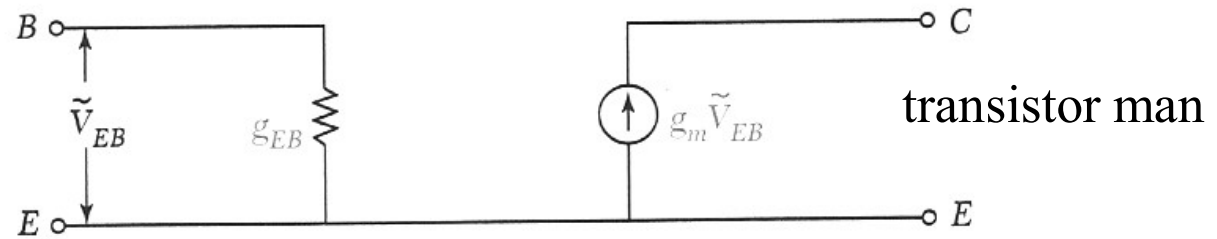
$$\tilde{i}_c = \beta \tilde{i}_B = \beta g_{EB} \tilde{v}_{EB}$$

input conductance:

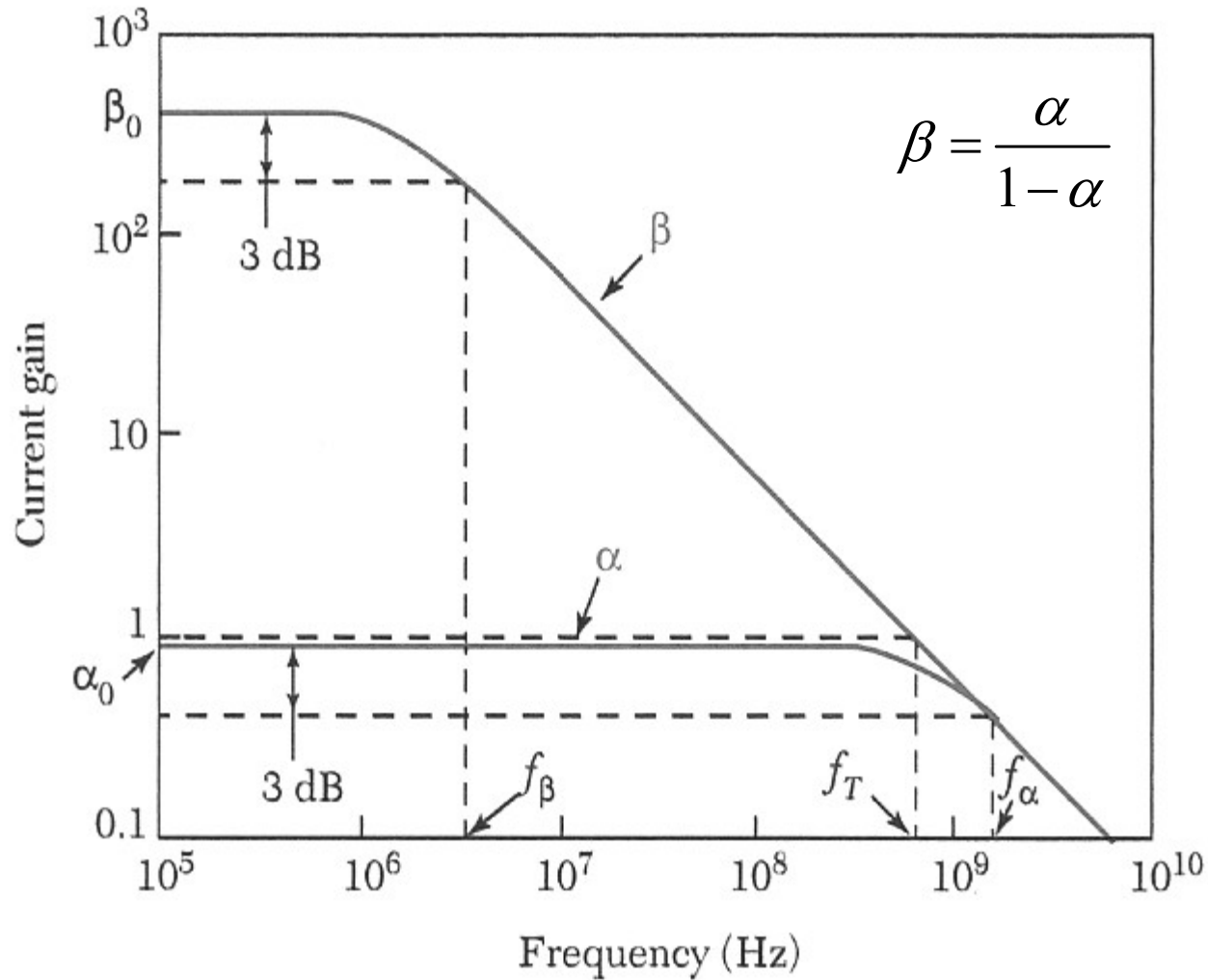
$$g_{EB} = \frac{\tilde{i}_B}{\tilde{v}_{EB}}$$

transconductance:

$$g_m = \frac{\tilde{i}_c}{\tilde{v}_{EB}}$$



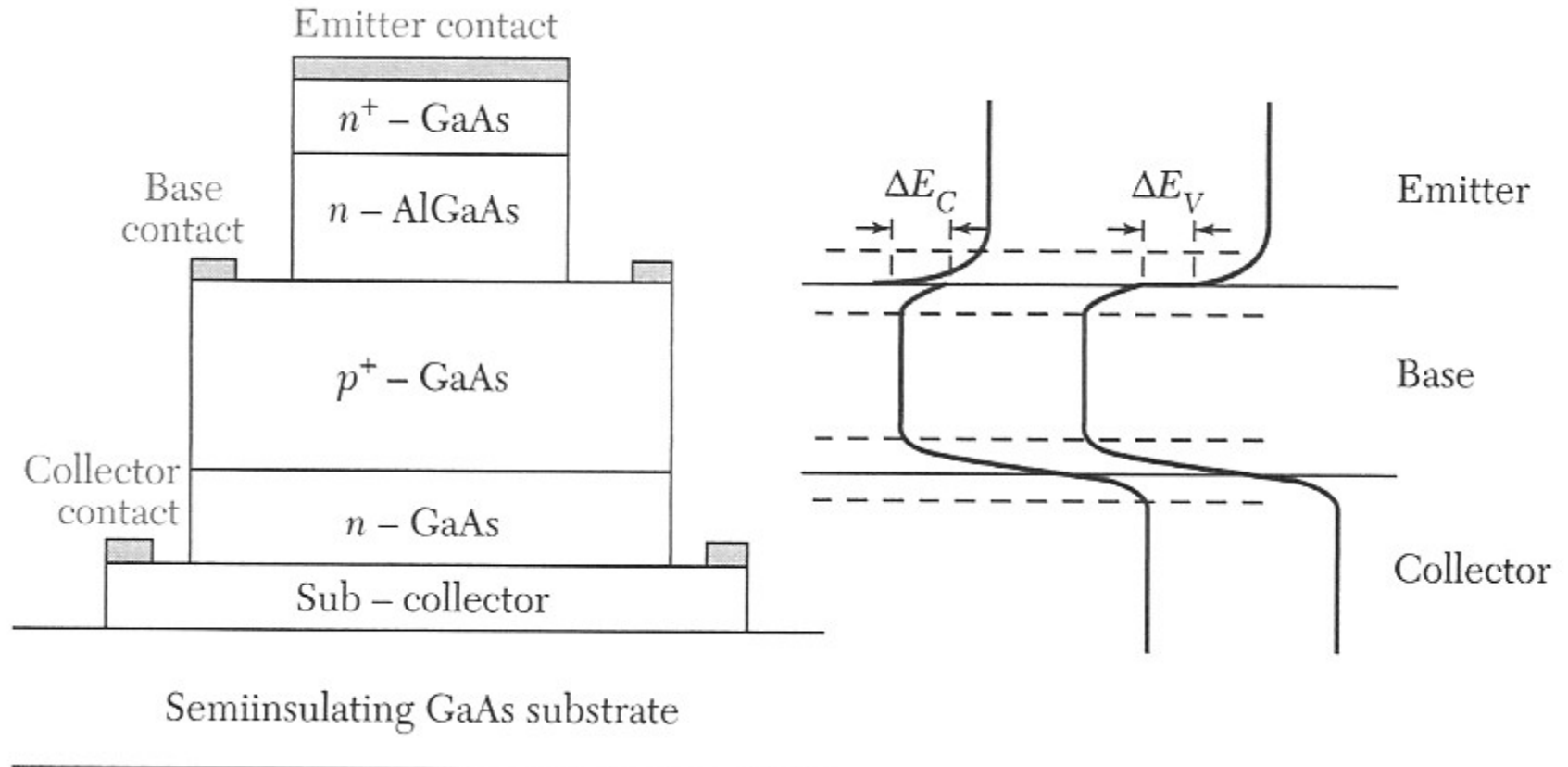
Small signal response



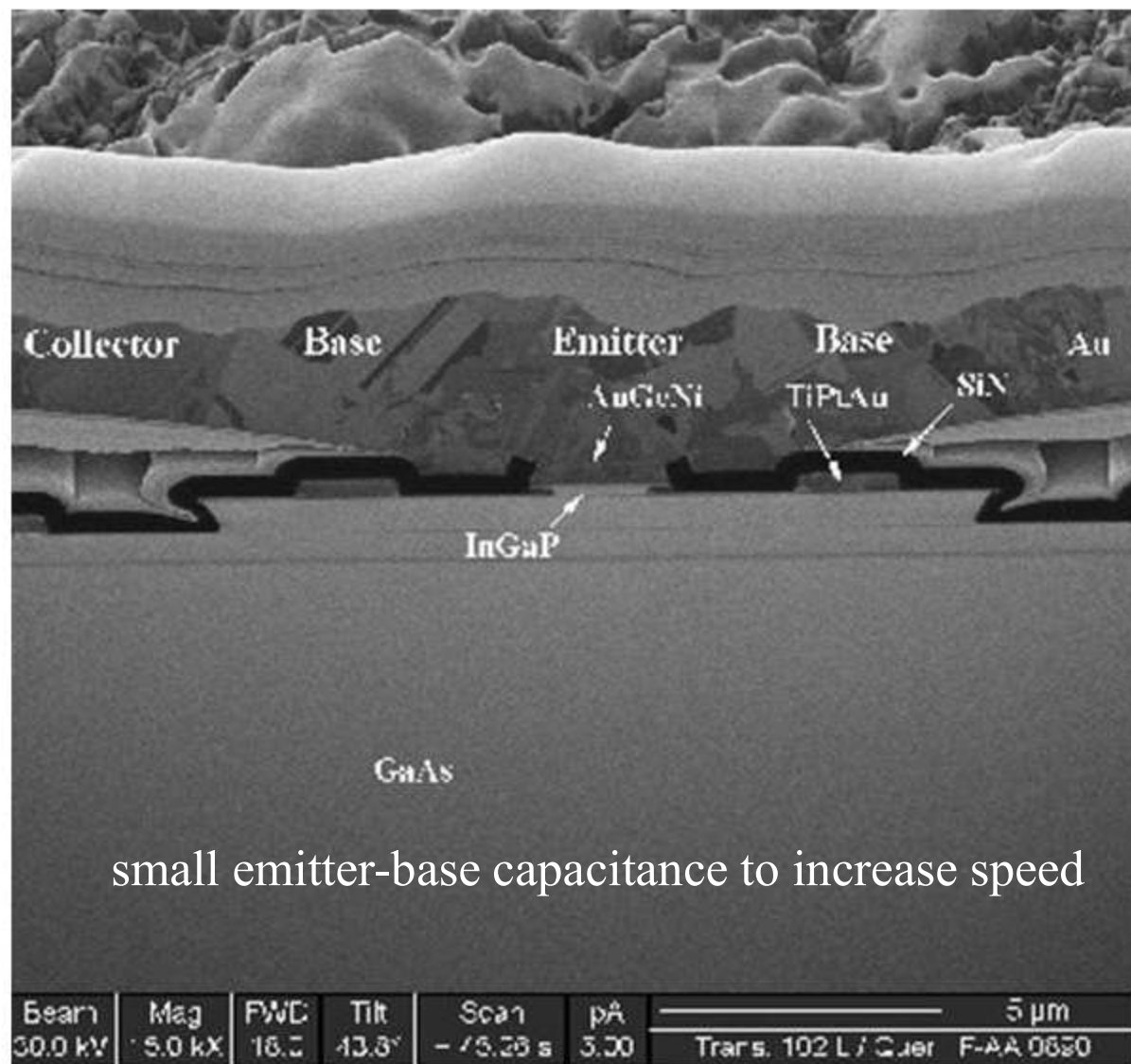
$$f_\beta = (1 - \alpha_0) f_\alpha$$

$$f_T = \alpha_0 f_\alpha$$

Heterojunction bipolar transistors



Heterojunction bipolar transistor



HBT current gain

$$I_C = \beta I_B$$

$$\beta = \frac{\alpha}{1-\alpha} \approx \frac{n_{B0}}{p_{E0}} \quad (\text{npn})$$

Higher doping in the emitter makes the minority carrier concentration lower in the emitter.

$$n_{B0} = \frac{n_i^2}{N_A} = \frac{N_C N_V \exp(-E_{gB} / k_B T)}{N_A}$$
$$p_{E0} = \frac{n_i^2}{N_D} = \frac{N'_C N'_V \exp(-E_{gE} / k_B T)}{N_D}$$

If the emitter and the base have different band gaps

$$\beta = \frac{N_E}{N_B} \frac{N_C N_V}{N'_C N'_V} \exp\left(\frac{\Delta E_g}{k_B T}\right) \sim 100000$$

HBT current gain

A HBT has an emitter bandgap of 1.62 and a base bandgap of 1.42.

A BJT has an emitter bandgap of 1.42 and a base bandgap of 1.42.

Both have an emitter doping of 10^{18} cm^{-3} and a base doping of 10^{15} cm^{-3} .

How much larger is the gain in the HBT?

$$\frac{\beta(\text{HBT})}{\beta(\text{BJT})} = \exp\left(\frac{\Delta E_g}{k_B T}\right) = \exp\left(\frac{1.62 - 1.42}{0.0259}\right) = 2257$$

Heavy doping narrows the bandgap so in a normal transistor the bandgap is smaller in the emitter.

HBT

Trade off gain for higher speed

Higher base doping

- lower base resistance

- reduced Early effect

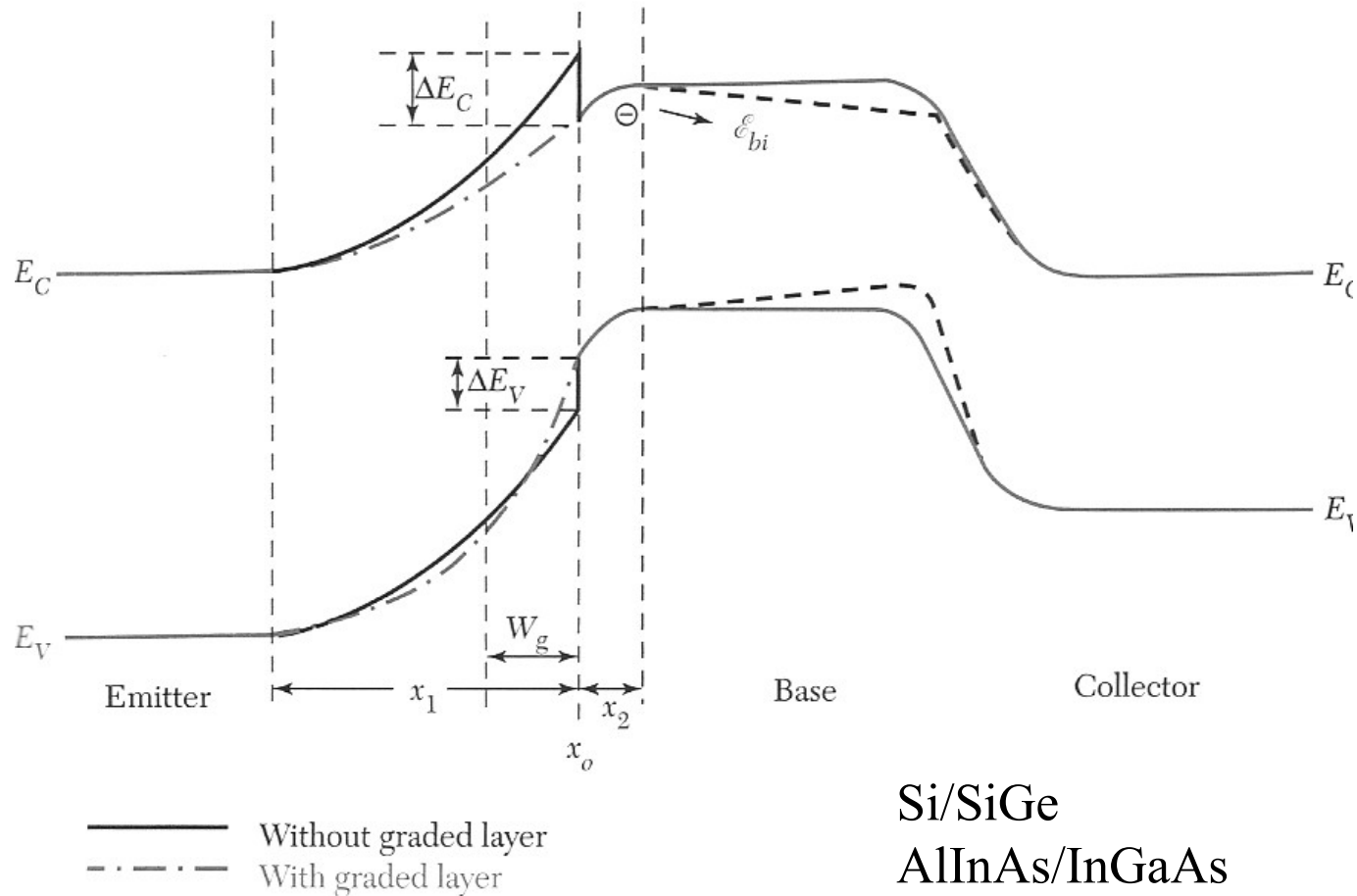
- less trouble with punch through

- base can be made thinner -> faster transistors

Because of higher base doping, a higher collector doping is possible without punchthrough

- lower collector resistance

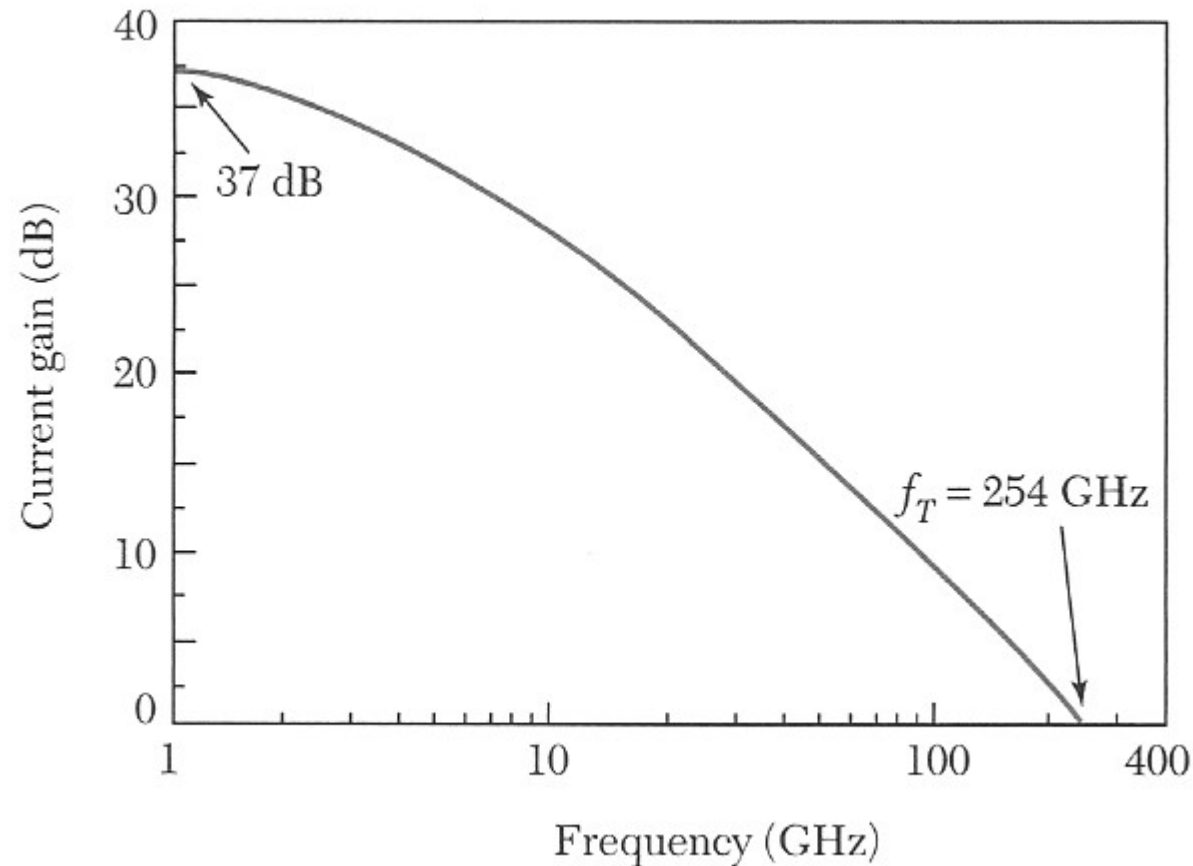
HBT current gain



band discontinuity reduces emitter efficiency

Graded layer emitter and base improve performance

Heterojunction bipolar transistors



Fastest InP/InGaAs HBT's have an f_T of 710 GHz.

Higher doping in the base allows for a thinner base without punch through and lower base resistance and thus higher frequency operation

Microwave engineering

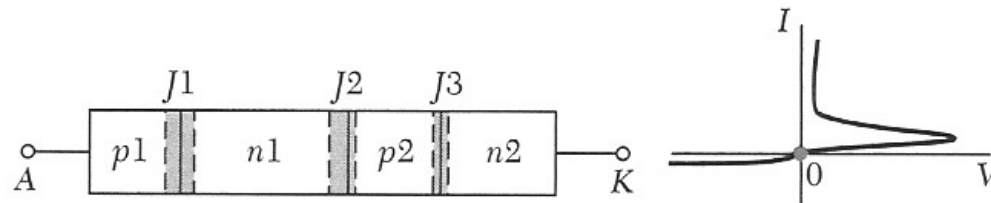
Electronics: $L \ll \lambda$ $f < \sim 10$ GHz

Microwave: $\lambda < L$ 10 GHz $< f < 1$ THz

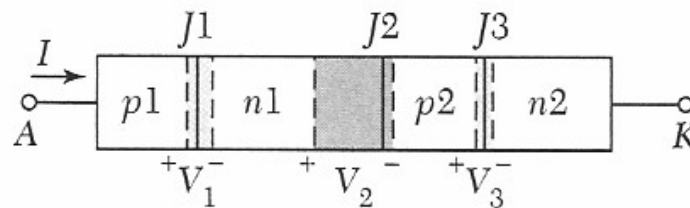
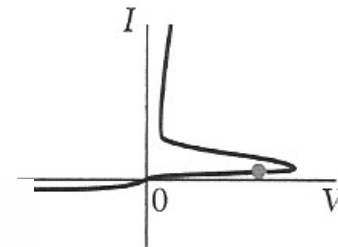
TeraHertz: $\lambda \ll L$ 1 THz $< f < 100$ THz

Optics: $\lambda \ll L$ 100 THz

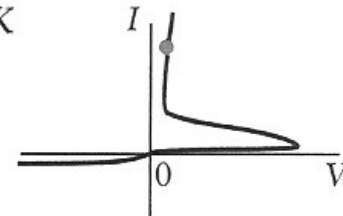
Thyristors



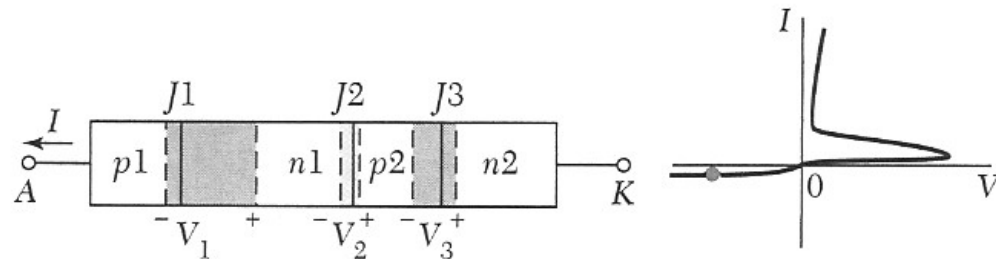
Forward blocking



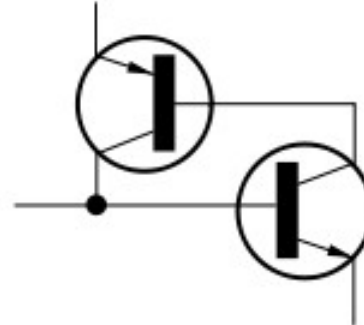
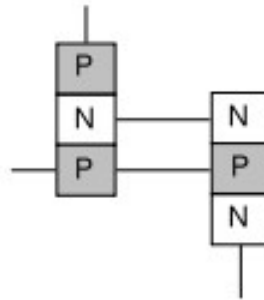
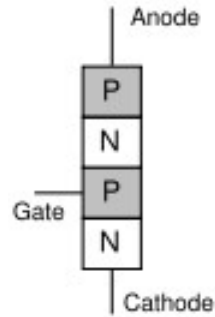
Forward conducting



Reverse blocking

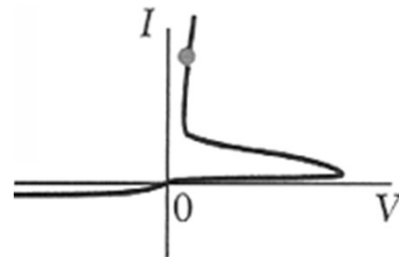


Thyristors

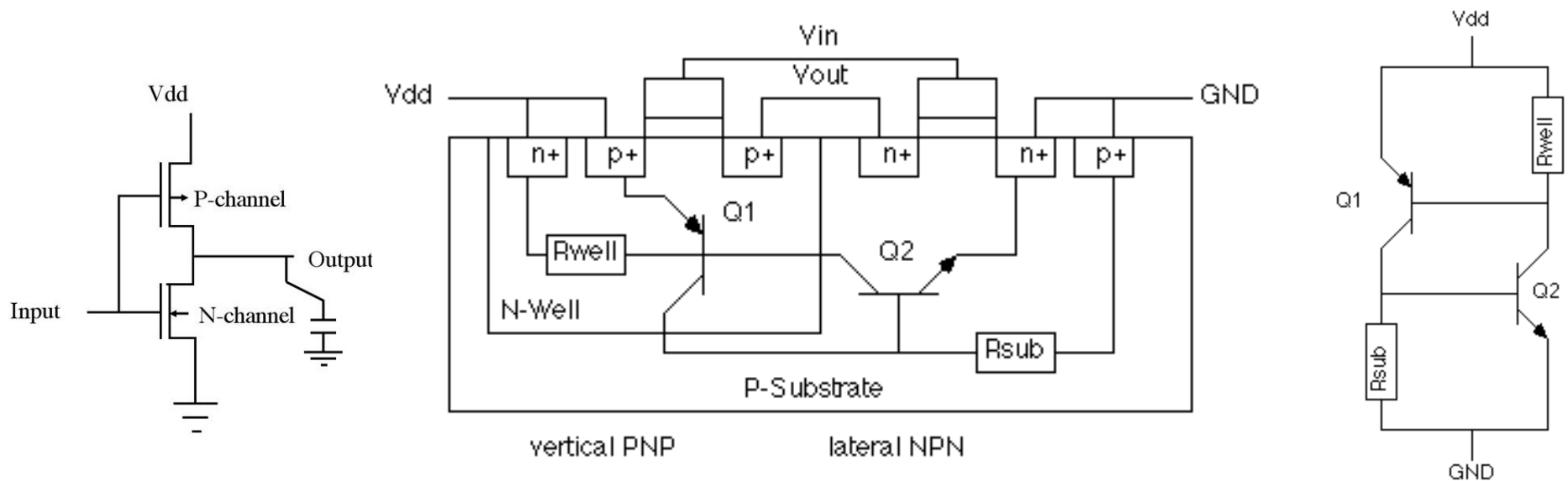


$$\beta_1 * \beta_2 > 1$$

Used for switching high currents or voltages



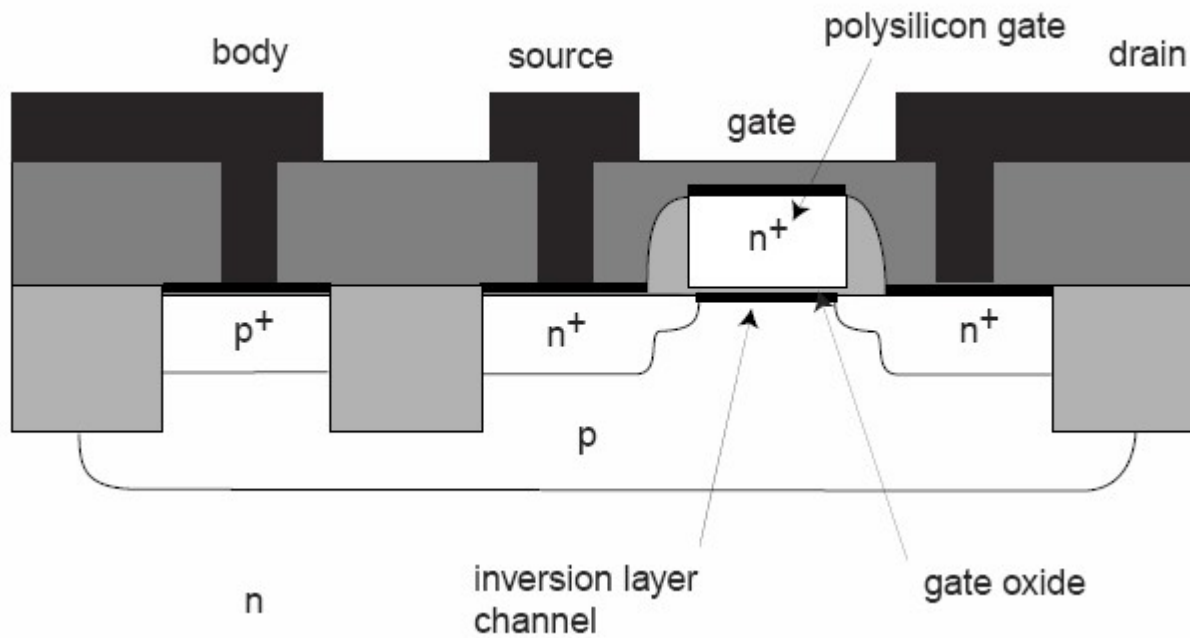
Latch-up



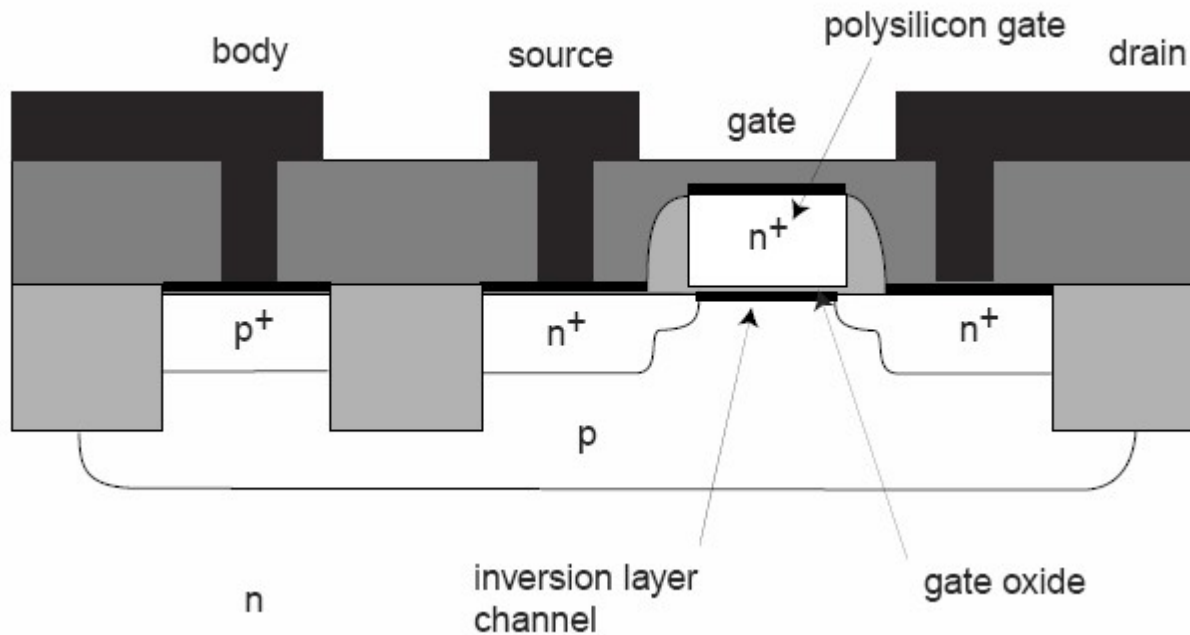
Both BJT's conduct, creating a low resistance path between V_{dd} and GND. The product of the gains of the two transistors in the feedback loop, is greater than one. The result of latchup is at the minimum a circuit malfunction, and in the worst case, the destruction of the device.

<http://www.ece.drexel.edu/courses/ECE-E431/latch-up/latch-up.html>

Can you operate like a BJT?



Subthreshold current

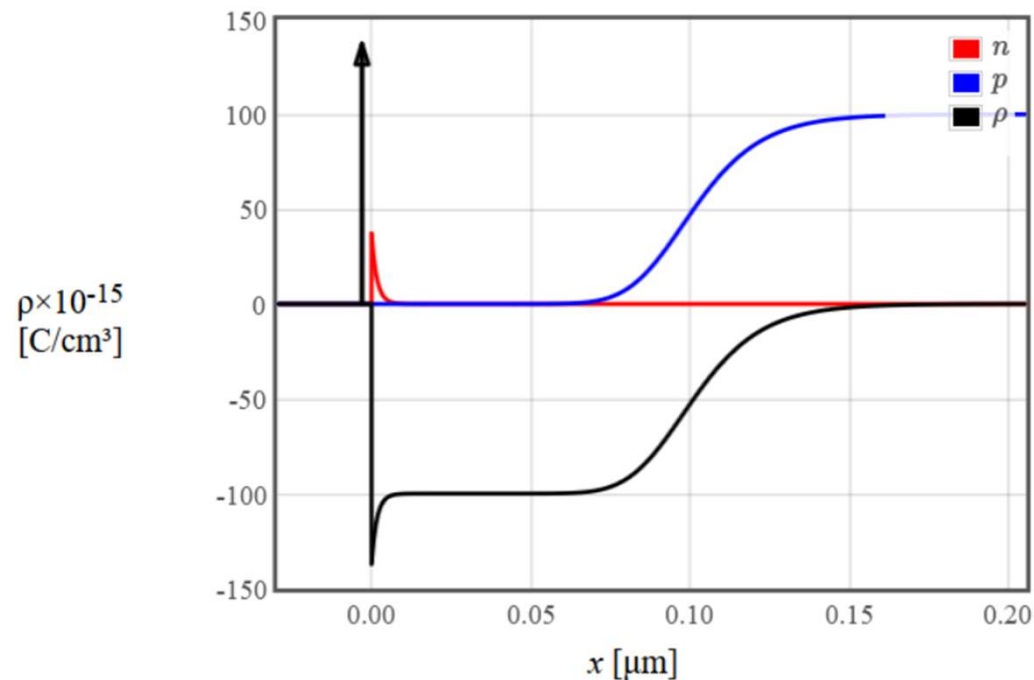


If the p-concentration in the channel is low, electrons emitted into the channel by the forward biased junction diffuse across the channel without recombining.

Subthreshold current – depletion approximation

$$x_p = -\frac{\epsilon_s}{\epsilon_{\text{ox}}} t_{\text{ox}} + \sqrt{\left(\frac{\epsilon_s}{\epsilon_{\text{ox}}} t_{\text{ox}}\right)^2 + \frac{2\epsilon_s}{eN_A} (V_g - V_{fb})}$$

$$n(x) = \begin{cases} \frac{n_i^2}{N_A} \exp\left(\frac{e^2 N_A (x_p - x)^2}{2\epsilon_s k_B T}\right) & \text{for } 0 < x < x_p, \\ \frac{n_i^2}{N_A} & \text{for } x > x_p, \end{cases}$$

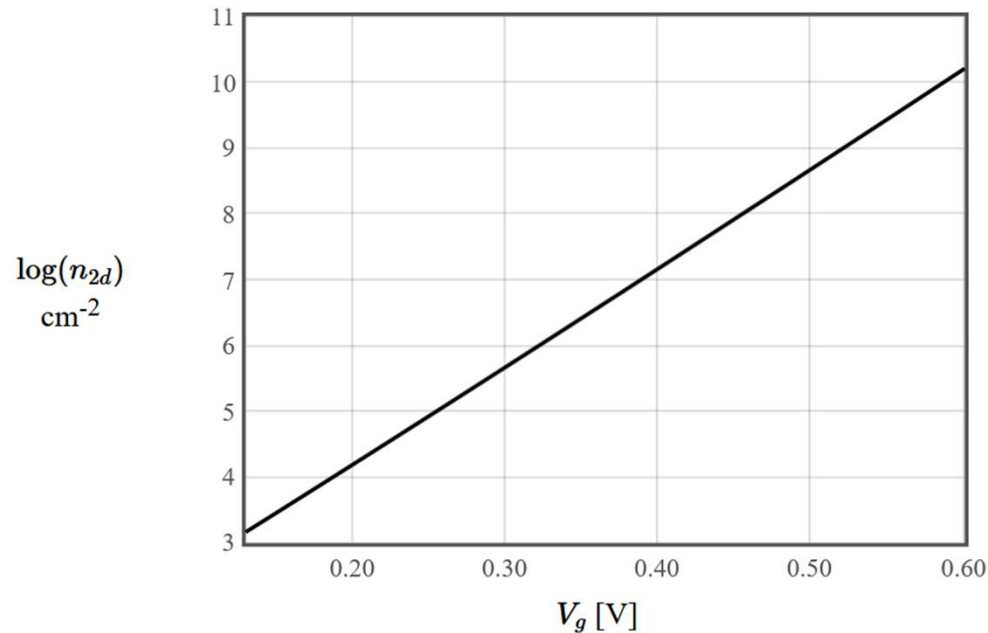


Subthreshold current – depletion approximation

$$n(x) = \frac{n_i^2}{N_A} \exp\left(\frac{e^2 N_A (x_p - x)^2}{2\epsilon_s k_B T}\right)$$

$$n(x) \approx \frac{n_i^2}{N_A} \exp\left(\frac{e^2 N_A (x_p^2 - 2x_p x)}{2\epsilon_s k_B T}\right)$$

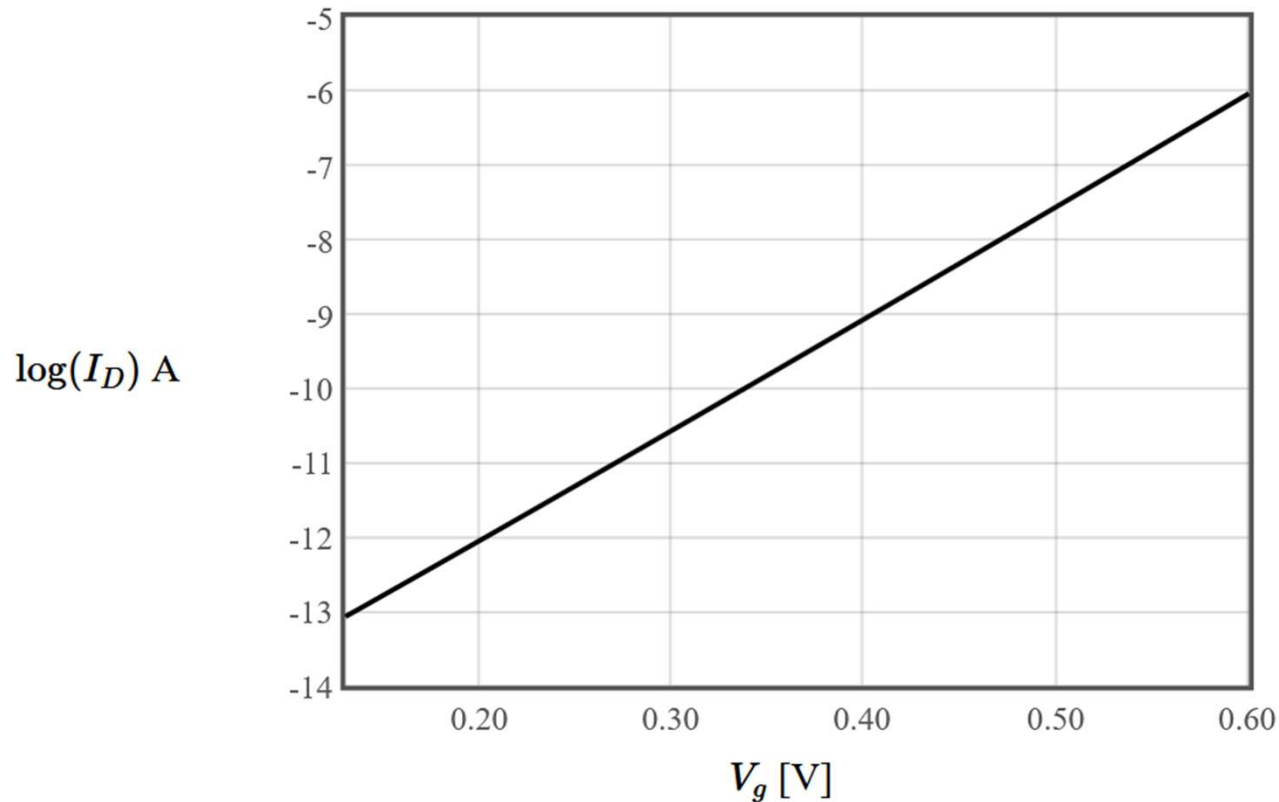
$$n_{2d} = \frac{n_i^2}{N_A} \exp\left(\frac{e^2 N_A x_p^2}{2\epsilon_s k_B T}\right) \frac{\epsilon_s k_B T}{e^2 N_A x_p}$$



Subthreshold current – depletion approximation

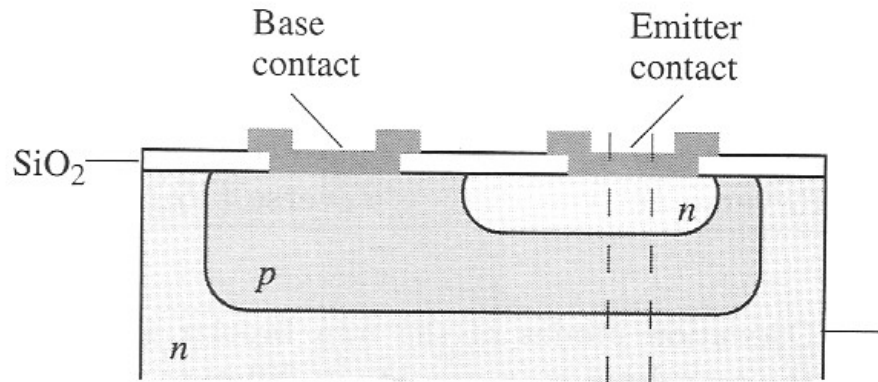
$$\nabla n \approx -\frac{n_{2d}}{L}$$

$$I_D \approx \frac{k_B T \mu W n_{2d}}{L} = \frac{n_i^2 \mu \epsilon_s k_B^2 T^2 W}{e^2 N_A^2 x_p L} \exp\left(\frac{e^2 N_A x_p^2}{2 \epsilon_s k_B T}\right)$$



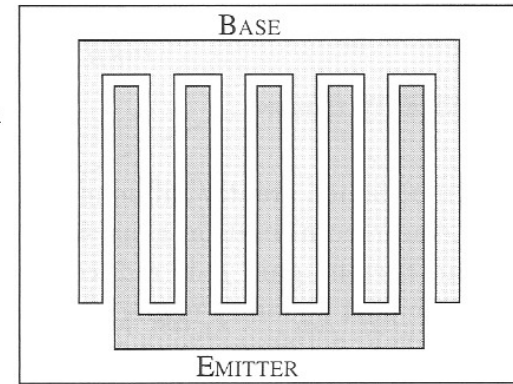
Subthreshold slope: 70-100 mV/decade

Interdigitated contacts in power transistors

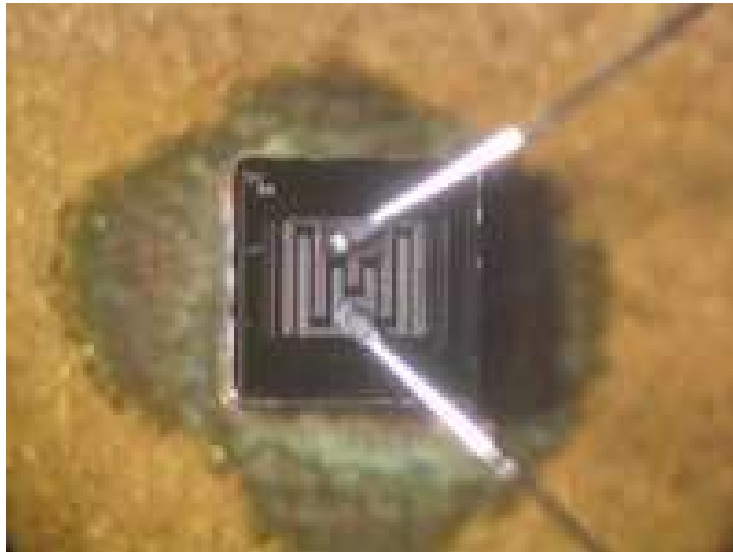
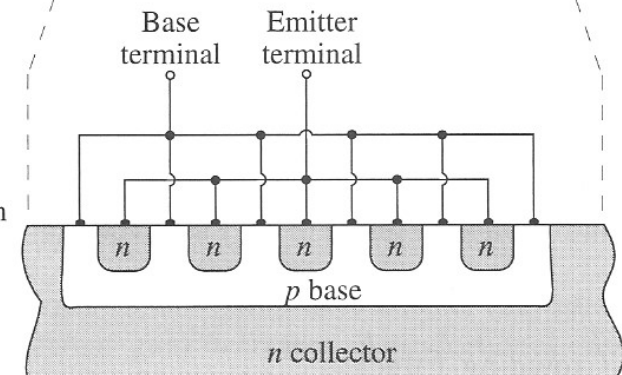


Interdigitated fingers to inject current uniformly into a bipolar device

Top view

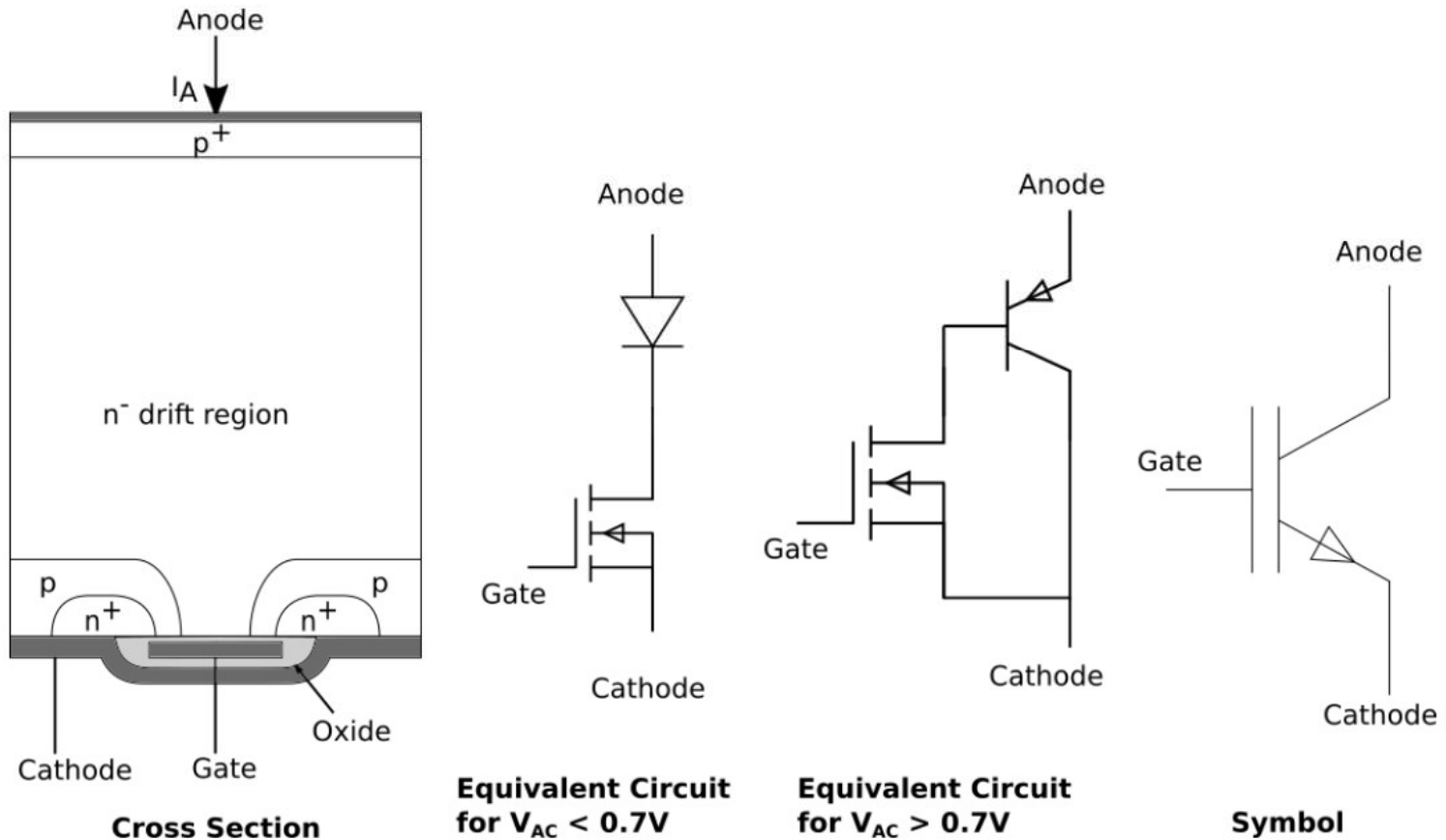


Cross-section



IGBT - Insulated Gate Bipolar Transistor

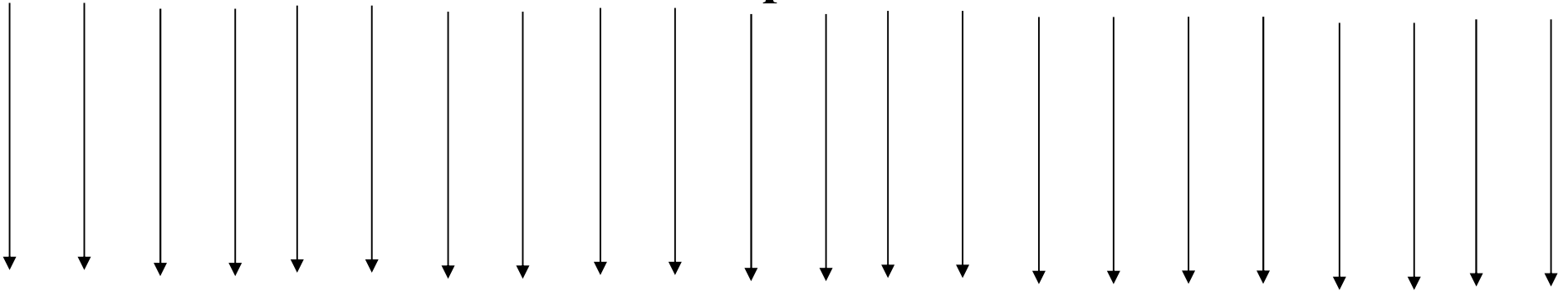
An IGBT is a combination of an insulated gate FET and a bipolar transistor. It is primarily used for switching high power loads



Used to switch large currents (in electric cars or trains).
Like a thyristor for high voltages.

<http://lampx.tugraz.at/~hadley/psd/L13/igbt.html>

Implant



SiO₂

Deposit oxide

Spin resist

Expose

Develop

Etch Oxide

Strip resist

Implant subcollector n+

p-Si

Antimony (Sb) has a low vapor pressure and won't evaporate during the subsequent CVD step

Epi-growth

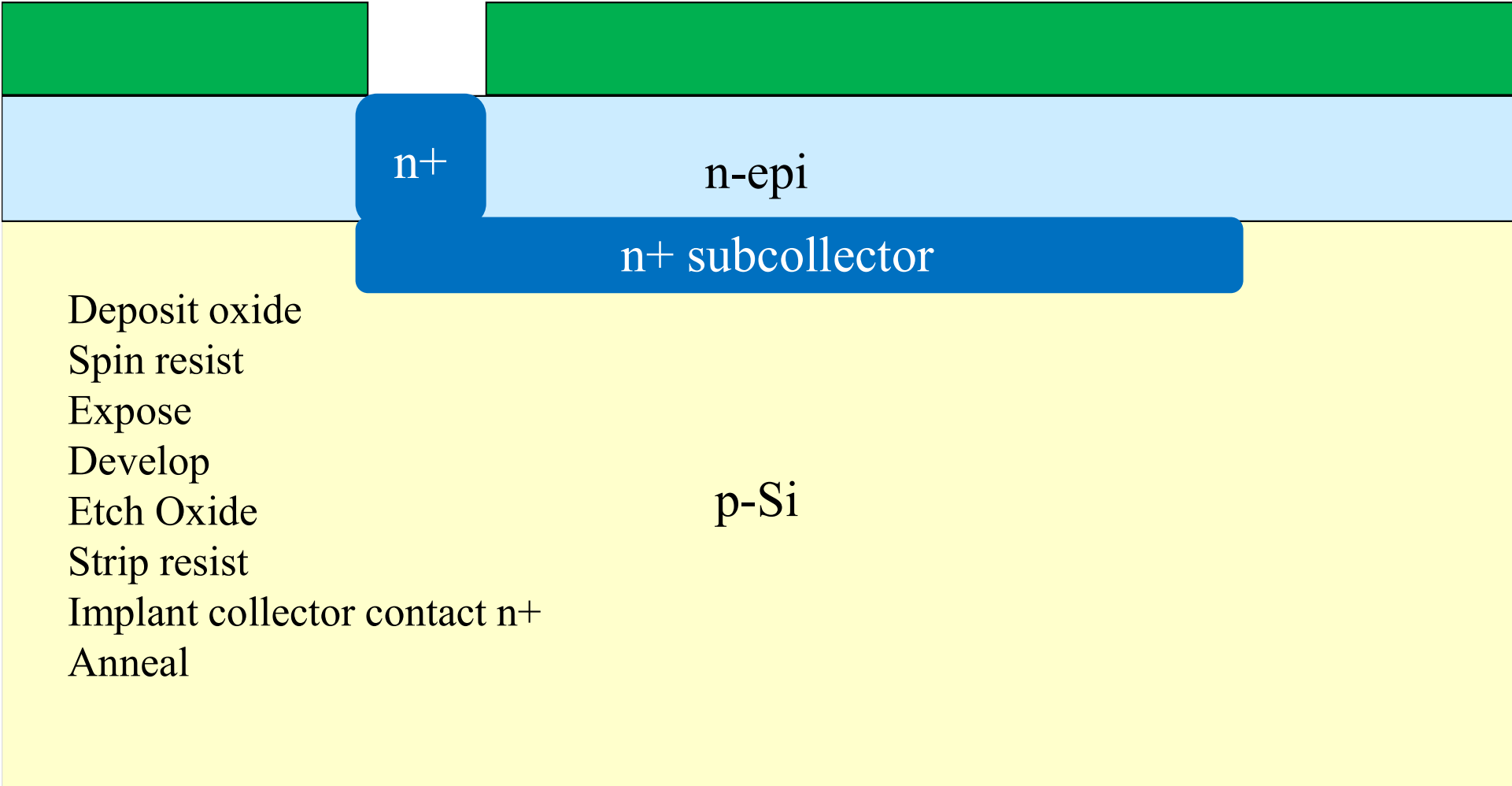
n-epi

n+ subcollector

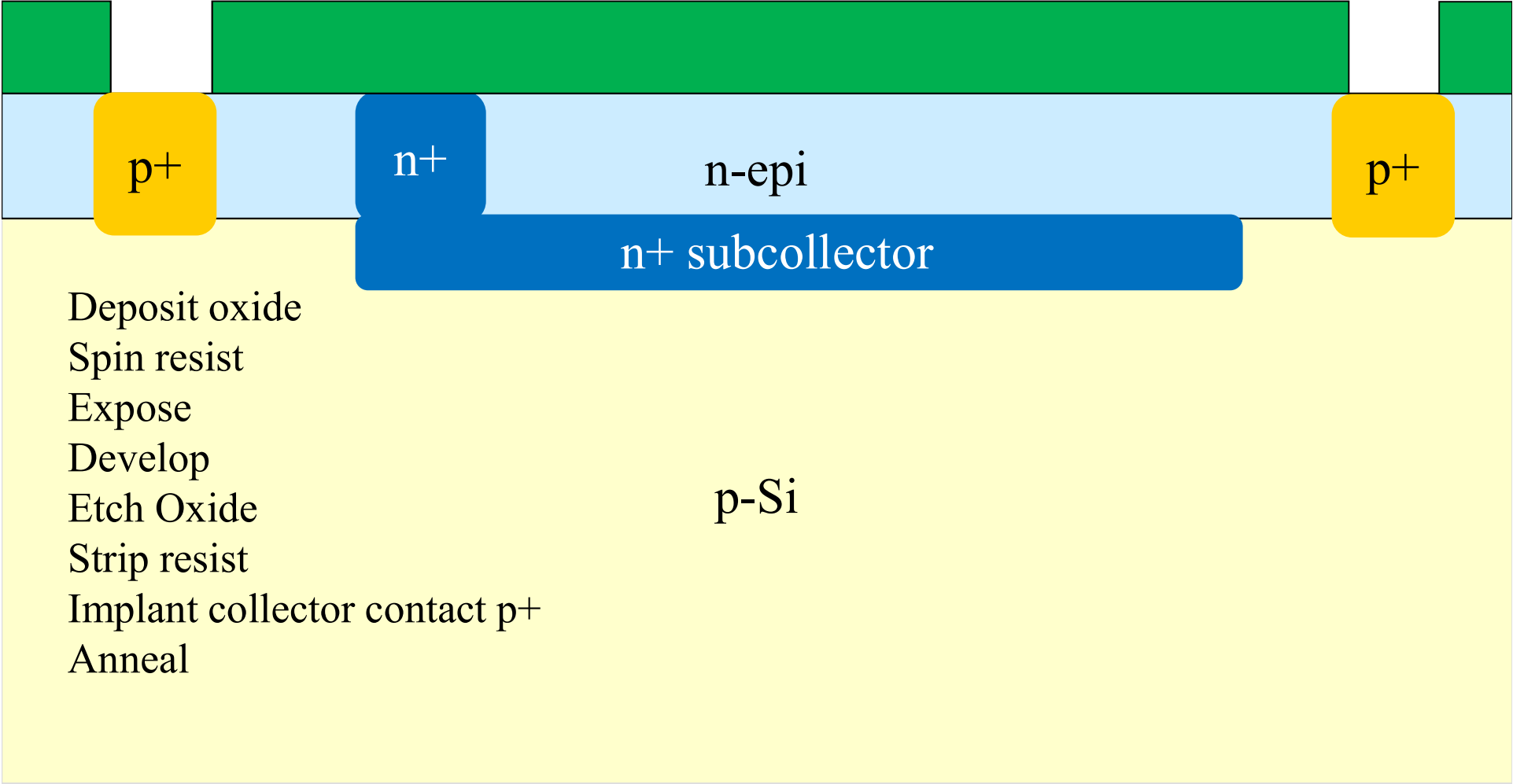
Remove oxide
Clean surface
Silicon epitaxy
CVD $\text{SiH}_4 + \text{PH}_3$

p-Si

Collector Contact

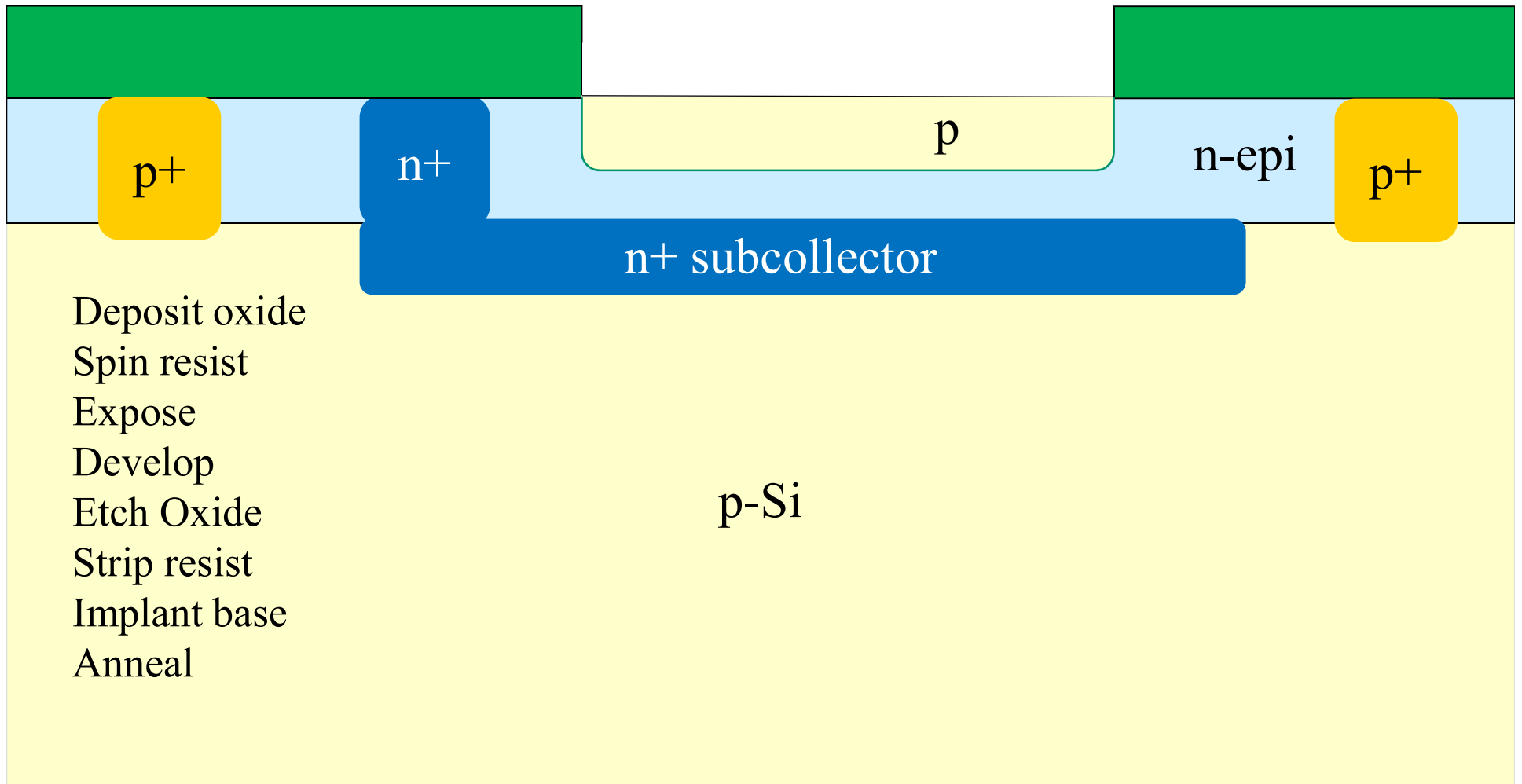


Guard ring



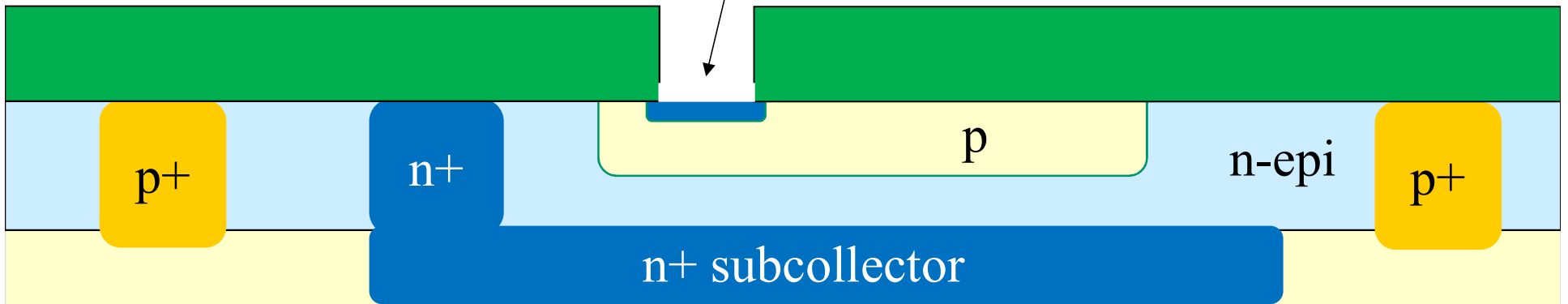
- Deposit oxide
- Spin resist
- Expose
- Develop
- Etch Oxide
- Strip resist
- Implant collector contact p+
- Anneal

p-well



- Deposit oxide
- Spin resist
- Expose
- Develop
- Etch Oxide
- Strip resist
- Implant base
- Anneal

n+ emitter



- Deposit oxide
- Spin resist
- Expose
- Develop
- Etch Oxide
- Strip resist
- Implant base
- Anneal

p-Si

BiCMOS

Only one additional step to CMOS is needed for BiCMOS

Bipolar junction transistors:
high speed
high gain
low output impedance
good for analog amplifiers

CMOS
high impedance
low power logic

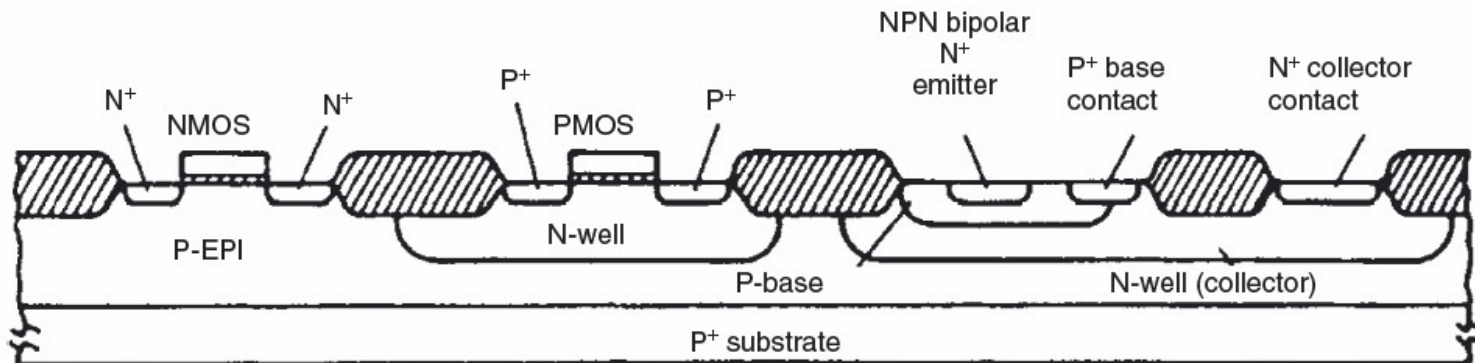
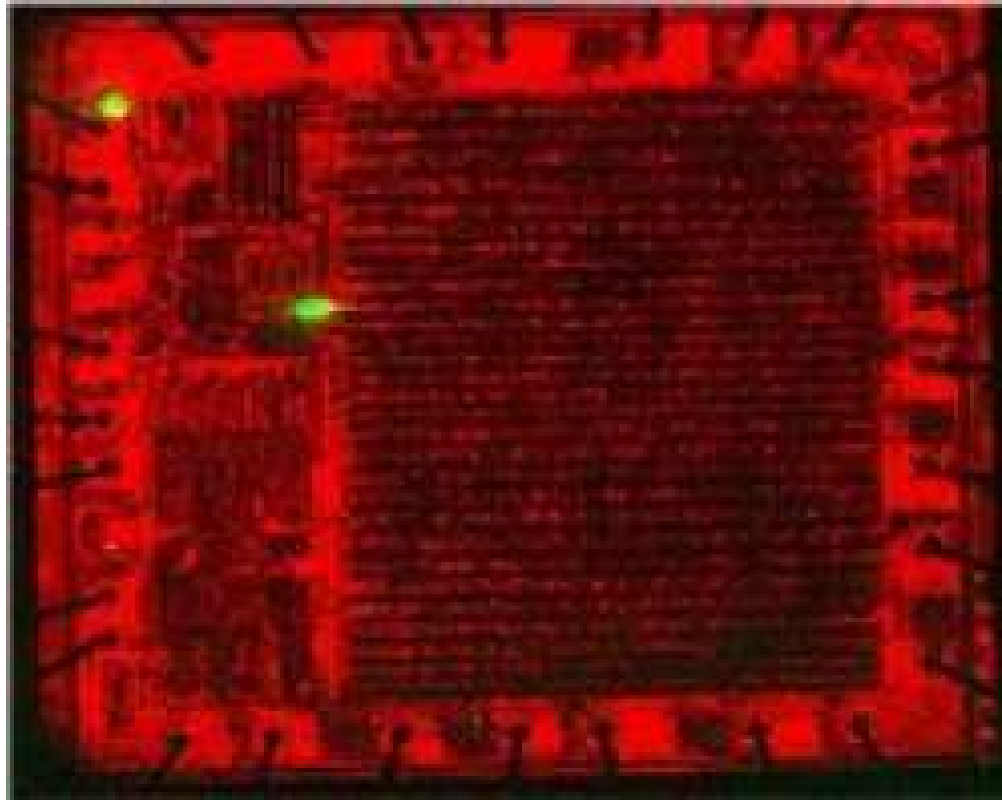


Figure 27.6 Simple BiCMOS technology: triple diffused-type bipolar transistor added to a CMOS process with minimal extra steps: only p-base diffusion mask is added to CMOS process flow. Reproduced from Alvarez (1989) by permission of Kluwer

Fransila

See: http://www.iue.tuwien.ac.at/phd/puchner/node48_app.html

Emission Microscope



Forward biased diodes emit light. (BJT)
Defects often emit light.

<http://www.muanalysis.com/techniques/emission-microscopy-emmi>

When does it emit light?

Thyristor

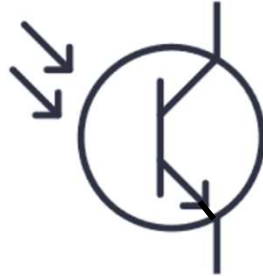
Bipolar junction transistors

MOSFET

JFET

Si diode

Phototransistor



What happens to all devices when you shine light on them? What if you make the devices out of direct band gap materials. Do they emit?